

On an error in defining temperature feedback

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KEYWORDS

Climate change · Climate modeling · Climate sensitivity
Dynamical systems · Control theory · Temperature feedback

ACKNOWLEDGEMENTS

The authors thank Mr William Bailey, Professor Freeman Dyson, Professor Chris Essex, Professor Dr Hermann Harde, Professor Dr Mojib Latif, Mr Nic Lewis, The Viscountess Monckton of Brenchley, Dr Benoît Rittaud, Academician Dr Vladimir Semenov, Professor Nir Shaviv, Dr Roger Taguchi, Mr George White and Academician Dr Nina Zaytseva for discussions, Professor Ray Bates, The Baron Clanmorris of Newbrook, Professor Will Happer, Dr David Heald, Mr William Rostron, Professor Murry Salby and the Global Warming Policy Foundation for pre-submission reviews; Mr Hal Shurtleff, Mr G. Edward Griffin, Ms Pamela Matlack-Klein, Professor Maria da Assunção Ferreira Pedrosa de Araújo, Professor Nils-Axel Mörner, the City Government of Moscow, the Heartland Institute, the Deutscher Bundestag and the Europäisches Institut für Klima und Energie for facilitating discussion at international conferences; and Professor Antonino Zichichi for having provided, at the Centre for Scientific Culture in Erice, Sicily, the high-level scientific forum from which these ideas sprang. Those acknowledged do not necessarily endorse the authors' conclusions. No author has received any specific funding for this work. A detailed conflict-of-interest declaration has been furnished to the editors.

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ABSTRACT

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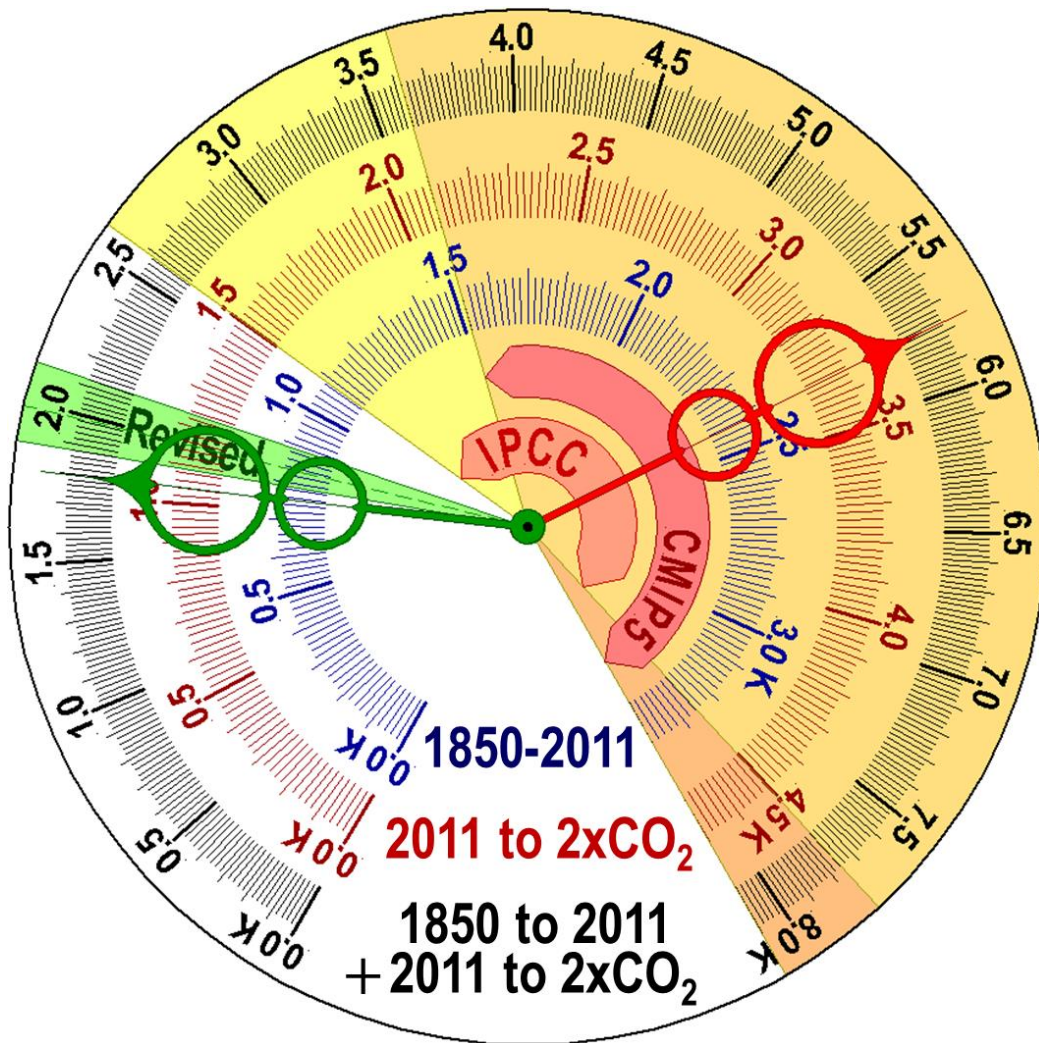
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CLIMATOLOGY, in borrowing feedback method from control theory, misapplies a concept from experimental science in an observational-science setting by defining temperature feedback as responding only to perturbations of reference temperature. One implication of this error is that, impossibly, the feedback fraction due to warming from noncondensing greenhouse gases exceeds that due to emission temperature by 1-2 orders of magnitude. Another implication is that feedback response constitutes up to 90% of midrange Charney sensitivity (equilibrium sensitivity to doubled CO₂ after feedback has acted) and of the uncertainty therein. In reality, feedback responds to the entire reference signal, which, in climate, is the sum of emission temperature and all natural as well as anthropogenic reference sensitivities. The system-gain factor, the ratio of equilibrium to reference temperatures and not (as now) of perturbations only, is insensitive even to large uncertainties in those temperatures. It was 1.1 in 1850 and in 2011. Revised Charney sensitivity, the product of the 1.05 K reference sensitivity to doubled CO₂ and the system-gain factor 1.1, falls on 1.15 [1.10, 1.25] K, confirmed empirically from ten published estimates of anthropogenic forcing. Monte Carlo simulations compared the CMIP5 and revised confidence intervals. An author and a government laboratory verified the theory with test apparatus. Current Charney-sensitivity projections on 3.35 [2.1, 4.7] K are excessive. Even without mitigation, global warming sufficient to cause net harm is unlikely.

1. Introduction

Global warming is not occurring as rapidly as predicted. The Intergovernmental Panel on Climate Change (IPCC 1990, pp. *xiii*, *xiv*) had projected $\sim 0.3 \pm 0.1$ K decade⁻¹ medium-term warming, but, after only 0.17 K decade⁻¹ was observed from 1990-2011 (HadCRUT4: Morice et al. 2012), for the first time IPCC (2013) replaced outputs from general-circulation models (GCMs) with its “expert judgment”, near-halving its medium-term projection to 0.17 ± 0.1 K decade⁻¹. However, IPCC did not reduce its [1.5, 4.5] K 95%-confidence interval of Charney sensitivity, the standard metric, which is equilibrium sensitivity to radiative forcing from doubled CO₂ after all temperature feedbacks of sub-decadal duration have operated. That interval remains as in Charney et al. (1979, p. 4), the first modern sensitivity study. The 3.35 [2.1, 4.7] K interval of projected Charney sensitivities in the fifth-generation models of the Climate Model Intercomparison Project (CMIP5: Andrews et al. 2012) is also excessive when compared with observed warming since 1850 (Fig. 1). Accordingly, the question whether there subsists a systemic error leading to much-overstated projections of global warming was investigated.



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FIG. 1. Overlapping projections by IPCC (2013) and CMIP5 (Andrews et al. 2012) of global warming from 1850-2011 (**blue scale**), in response to doubled CO₂ (**red scale**) and the sum of these two (**black scale**) greatly exceed warming equivalent to the 0.75 K observed from 1850-2011 (HadCRUT4: **green needle**). The 3.35 K CMIP5 mid-range Charney sensitivity (**red needle**) implies 2.4 K anthropogenic warming by 2011, about thrice observation. The revised warming interval derived herein (**pale green region**) is consistent with observed warming to 2011 (**green needle**).

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The small uncertainty of $\pm 10\%$ (IPCC 2013, p 676, §8.3.2.1; cf. Cess et al. 1993) in reference sensitivity (sensitivity before allowing for temperature feedback) and the large uncertainty in the feedback response indicate that, if there be some such error, it may lie in the treatment of temperature feedback. IPCC (2013) indicates the significance of feedback by mentioning it more than 1000 times. Midrange feedback response is currently thought to account for some 85% (Vial et al. 2013) of the 3 K uncertainty in equilibrium sensitivity (sensitivity after feedback has acted), while feedback is currently thought to contribute 70% [50%, 90%] of equilibrium sensitivity. Uncertainty in feedback strength arising from an error in the definition of temperature feedback will be shown to be the chief reason why the published intervals of projected Charney sensitivity (IPCC 2013) remain broad and have resisted constraint for 40 years, leading to a threefold overstatement of projected midrange global warming.

88 **2. Erroneous definition of temperature feedback**

89 Feedback in dynamical systems is correctly defined (Black 1934, Bode 1945, Roe 2009) as responding
90 to the entire reference signal, which is the sum of the input signal (in climate, emission temperature)
91 and any perturbations thereof (reference sensitivities to natural as well as anthropogenic perturbations).
92 This long-established definition had its origin in electronic network analysis, from which sprang the
93 branch of engineering physics known as control theory. For a century, it has been so often applied to
94 dynamical systems throughout the sciences, from telephone circuits to rocketry, as to be unimpeachable.

95 Feedback theory has long been incorporated into climatology by explicit reference to its origin in
96 electronics (e.g. Hansen et al. 1984; Schlesinger 1985, IPCC 1990 p. *xiv*, Roe 2009, Schmidt et al. 2010,
97 Monckton of Brenchley 2015b). However, climatology erroneously defines feedback as responding to
98 perturbations only; the definition does not encompass feedback response to emission temperature.

99 Feedback is at once a consequence and an instrument of causality. In physics, natural laws describe
100 the evolution and interaction of quantities – measurable properties of the universe at a particular point
101 in space-time. Causality describes the direction of their interaction and evolution. If a system is
102 sufficiently complex, causal interactions may take the form of chains and even loops, such as the
103 feedback loop. Little complexity is required as a condition for the establishment of a causal loop. For
104 instance, a solid at 0 K upon which a constant source of radiation is incident will at first absorb more
105 energy than it emits. The difference will warm the solid, diminishing the radiative imbalance and
106 slowing the rate of warming. Eventually, radiative equilibrium will be attained and the solid will hold
107 its new temperature. Bony et al. (2006), describing this feedback process as “the most important
108 feedback in the climate system”, imply that at least one feedback will operate at any given temperature.

109 Feedbacks are an emergent phenomenon. Therefore, they may not be arbitrarily defined. Since
110 causality is a universal property, the feedback principles underlying that causality are universal
111 properties applicable to all dynamical systems, from electronic circuits to climate.

112 Where an approximately constant radiative input acts upon a dynamical system, three outcomes are
113 possible. First, where the output is constant and exceeds the input, any feedback processes that are
114 present will have responded to the input by amplifying the output. Secondly, where the output is
115 constant and less than the input, the feedback processes will have responded to the input by attenuating
116 the output. Thirdly, where the system is unstable, the output will never have attained a constant value.

117 In the Earth’s climate, the observed global mean surface temperature at any time exceeds the
118 reference temperature that would hypothetically obtain without feedback. Accordingly, net-positive
119 temperature feedback processes subsist, amplifying the reference temperature. At any given time t at
120 which the climate is in radiative equilibrium (or at which due adjustment for any radiative
121 disequilibrium at time t establishes a theoretical equilibrium), **reference temperature R_t** is defined as
122 the absolute temperature that would obtain in the absence of feedback. **Equilibrium temperature E_t** is

123 defined as the absolute temperature that obtains once the climate has returned to equilibrium after
 124 short-acting feedbacks have acted upon R_t . Thus, E_t is a function $E(R)$ of R_t .

125 *Ex definitione*, the **absolute system-gain factor** A_t , which is the function $A(E, R)$ of E_t, R_t that
 126 encompasses the entire operation of temperature feedback at any time t of radiative equilibrium, is the
 127 ratio of E_t to R_t (Eq. 1); and A_t thus derived applies regardless of the shape of the function $E(R)$.

$$A_t := E_t/R_t \quad | \quad \text{Absolute system-gain factor} \quad (1)$$

$$a_t := \Delta E_{t-1}/\Delta R_{t-1} \quad | \quad \text{Partial system-gain factor} \quad (2)$$

$$A_t \leq a_t \quad | \quad \text{At radiative equilibrium} \quad (3)$$

128 Climatology has hitherto eschewed the absolute system-gain factor A_t , preferring to rely
 129 exclusively upon the **partial system-gain factor** a_t , the function $a(\Delta E, \Delta R)$ of equilibrium sensitivity
 130 ΔE_{t-1} , which is the ratio of **equilibrium sensitivity** ΔE_{t-1} to **reference sensitivity** ΔR_{t-1} (Eq. 2).

131 Originally, GCMs' outputs served as the inputs to a separate, simple model incorporating Eq. (2),
 132 from which equilibrium sensitivities were derived. Though GCMs now derive equilibrium sensitivities
 133 without reference to Eq. (2), it has hitherto escaped attention that such feedback processes as subsist in
 134 the climate at time t must perforce act upon the entire reference temperature R_t , and not merely upon
 135 some arbitrarily-chosen perturbation ΔR_{t-1} . Since the absolute temperatures E_t, R_t whose ratio is A_t
 136 exceed by two orders of magnitude the sensitivities $\Delta E_{t-1}, \Delta R_{t-1}$ whose ratio is a_t , even large
 137 uncertainties in E_t, R_t entail only a small uncertainty in A_t . By contrast, even small uncertainties in
 138 $\Delta R_{t-1}, \Delta E_{t-1}$ entail a large uncertainty in a_t . This is the chief reason why constraint of equilibrium
 139 sensitivity has hitherto proven elusive. Eq. (1) permits a considerably tighter and more reliable
 140 constraint of equilibrium sensitivities ΔE_{t-1} than Eq. (2).

141 Though differentiation tends to increase signal noise owing to high-pass behavior, the uncertainty
 142 introduced by this consideration is small because, as will be shown, if the shape of the function $E(R)$ is
 143 exponential the exponent x barely exceeds unity, so that the equilibrium-response function $E(R)$ is
 144 near-linear. For this reason, at any time t when the climate is in equilibrium, $A_t < a_t$ where $E(R)$ is a
 145 growth function, while $A_t = a_t$ where $E(R)$ is linear (Eq. 3).

146 Eqs. (4-6) demonstrate the relationship between the two system-gain factors A, a_t .

$$E_t = R_t A_t \quad | \quad \text{At equilibrium} \quad (4)$$

$$E_{t-1} = R_{t-1} A_{t-1} \quad | \quad \text{At previous equilibrium} \quad (5)$$

$$\begin{aligned} \Delta E_{t-1} &= E_t - E_{t-1} = R_t A_t - R_{t-1} A_{t-1} & | \quad \text{Eq. (4) - Eq. (5):} & (6) \\ &= (R_t - R_{t-1}) a_t = \Delta R_{t-1} a_t & | \quad \text{partial system-gain equation} \end{aligned}$$

147 From Eq. (2) and empirical data, a_t may be estimated via Eq. (7). However, even though E_t, R_t in
 148 1850 are well constrained, there is considerable uncertainty as to their values thereafter. Therefore, Eq.
 149 (7) has not proven useful hitherto, and the broad interval of projected equilibrium sensitivities has
 150 resisted constraint.

$$a_t = \frac{E_t - E_{t-1}}{R_t - R_{t-1}} = \frac{\Delta E_{t-1}}{\Delta R_{t-1}} \quad | \quad \text{Eq. (4) - Eq. (5)} \quad (7)$$

151 GCMs derive a_t independently of Eqs. (1, 2). They simulate physical processes that give rise to
 152 temperature feedbacks, treating them as an emergent property diagnosed from models' outputs (Soden
 153 & Held 2006; Vial et al. 2013). They attempt to derive the partial system-gain factor a_t bottom-up by
 154 estimating the individual climate-relevant temperature feedbacks, treating a_t (Eq. 2) as the ratio solely
 155 of sensitivities $\Delta E_{t-1}/\Delta R_{t-1}$ but not also as the ratio (Eq. 1) of absolute temperatures E_t/R_t .

156 Eqs. (4-6) may be represented by a leading-order Taylor-series expansion, Eq. (10), derived via
 157 Eqs. (8, 9) (Bony et al. 2006, Roe 2009).

$$E_t - E_{t-1} = (R_t - R_{t-1}) a_t \quad | \quad \text{Rearrange Eq. (7)} \quad (8)$$

$$E_t = E_{t-1} + (R_t - R_{t-1}) a_t \quad | \quad \text{Transpose } E_{t-1} \quad (9)$$

$$E_t(R) = E_{t-1}(R) + (R_t - R_{t-1}) dE/dR \quad | \quad \text{Taylor-series expansion} \quad (10)$$

158 Either Eq. (1) or Eq. (2) may be used diagnostically to derive ΔE_t from specified values of $\Delta R_t, A_t$,
 159 provided that A_t has first been correctly derived. However, derivation of Eq. (2) from the energy-
 160 balance equation via a Taylor-series expansion reveals nothing of the magnitude of the system-gain
 161 factor. That factor is reliably constrainable only via Eq. (1).

162 The definition of “climate feedback” in IPCC (2013, p. 1450) does not state that feedback processes
 163 respond to absolute reference temperature. Instead, *perturb* or *perturbation* is mentioned five times.
 164 Climatology's definition is consistent with Eq. (2) but is so restrictive as to be inconsistent with Eq. (1).

165 “**Climate feedback:** An interaction in which a *perturbation* in one climate quantity causes a
 166 change in a second, and the change in the second quantity ultimately leads to an additional
 167 change in the first. A negative feedback is one in which the initial *perturbation* is weakened by
 168 the changes it causes; a positive feedback is one in which the initial *perturbation* is enhanced.
 169 In this Assessment Report, a somewhat narrower definition is often used in which the climate
 170 quantity that is *perturbed* is the global mean surface temperature, which in turn causes changes
 171 in the global radiation budget. In either case, the initial *perturbation* can either be externally
 172 forced or arise as part of internal variability.” [Authors' emphases]

173 The error here is that the difference between a pre-existing reference temperature and a
 174 perturbation thereof is an artefact. Physics does not pass judgment on different states of the same
 175 quantity: they are as they are. To call one state a quantity and another state a perturbation is a value-
 176 judgment by the observer. If one were to define the initial reference temperature as 0 K, then every
 177 temperature > 0 K would be a perturbation of that reference temperature. Accordingly, climatology's
 178 definition is not of universal application, since the results of relying upon it depend on an arbitrary
 179 value defined as “quantity”. Climatology's definition is erroneous: it fails to take advantage of the
 180 absolute system-gain factor A_t , derived in Eq. (1), which reliably constrains equilibrium sensitivities.

181 From GCMs' outputs, n individual temperature feedbacks $(\lambda_i)_t$ in $W\ m^{-2}\ K^{-1}$, summing to $\lambda_t =$
 182 $\sum_{i=1}^n (\lambda_i)_t$, are diagnosed. Where reference sensitivity ΔR_{t-1} is the product of a radiative forcing ΔQ_{t-1}
 183 and the Planck sensitivity parameter P_t (Eq. 15), Eq. (11) gives equilibrium sensitivity ΔE_{t-1} .

$$\Delta E_{t-1} = [\Delta Q_{t-1} + \lambda_t \Delta E_{t-1}] P_t = \frac{\Delta Q_{t-1} P_t}{1 - \lambda_t P_t} = \frac{\Delta R_{t-1}}{1 - f_t} = \Delta R_{t-1} a_t. \quad (11)$$

184 IPCC (2007, p. 631 fn.) describes Eq. (11) thus [after adjusting notation to conform hereto]:

185 “... the amplification [a_t] of the global warming from a feedback sum [λ_t] (in $W\ m^{-2}\ K^{-1}$) with
 186 no other feedbacks operating is $[1/(1 - \lambda_t P_t)]$, where [P_t] is [~ 0.3 , the reciprocal of] the ‘uniform
 187 temperature’ radiative cooling response (of value approximately $3.2\ K\ W^{-1}\ m^2$: Bony et al. 2006).
 188 If n independent feedbacks operate, [λ_t] is replaced by $[(\lambda_1)_t + (\lambda_2)_t + \dots + (\lambda_n)_t]$.”

189 As a direct result of climatology's error in defining temperature feedback, it has hitherto been
 190 implicitly assumed that feedbacks do not respond to reference temperature R_1 as it stood in 1850: see
 191 e.g. Hansen et al. (1981), Schlesinger (1985), IPCC (1990, p. *xiv*), Roe (2009), Schmidt et al. (2010).
 192 Attempts at bottom-up diagnosis using the partial system-gain factor a_t have led to large
 193 overstatements of the feedback fraction f_t , of the feedback response $b_t (= f_t E_t = E_t - R_t)$, of the
 194 system-gain factors $A_t (= E_t/R_t)$, $a_t (= \Delta E_{t-1}/\Delta R_{t-1})$ and thus of all equilibrium sensitivities ΔE_{t-1} .

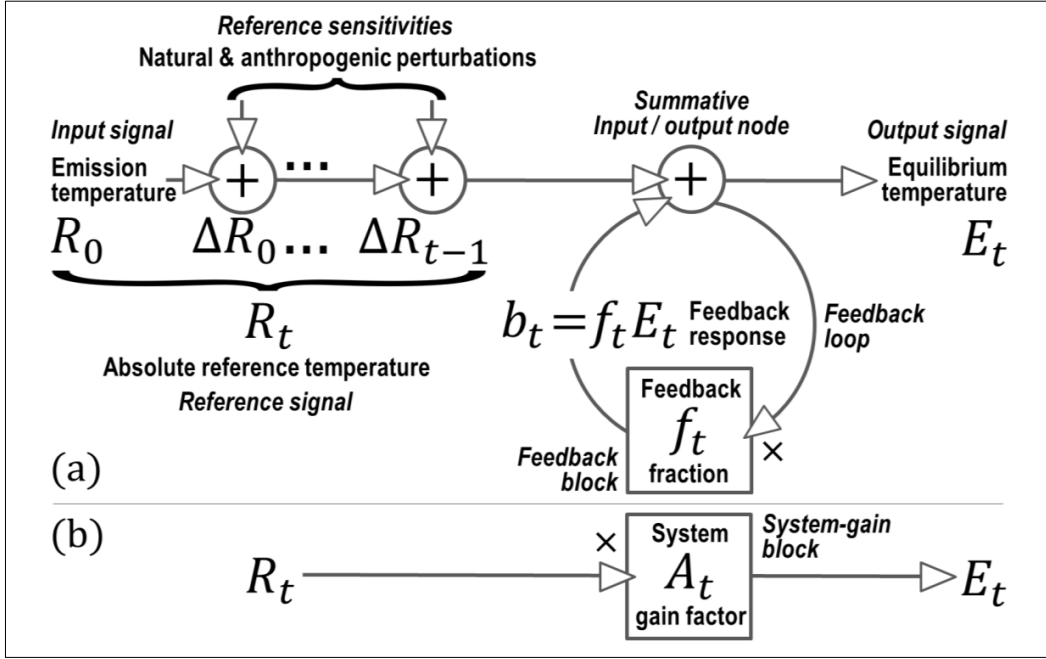
195 The consequences of the error of definition are severe. It is currently thought that, owing to
 196 feedback, equilibrium sensitivity ΔE_{t-1} exceeds reference sensitivity ΔR_{t-1} by up to fourfold; in some
 197 sources, up to tenfold (e.g. Armour 2017; Friedrich et al. 2016; Johansson et al. 2015; Murphy et al.
 198 2009; Forest et al. 2006; Andronova & Schlesinger 2001).

199 3. Definition of temperature feedback and related terms

200 Formal definitions of temperature feedback and related terms and a demonstration of the form of
 201 the system-gain factor A_t are essential. From the revised definitions, a corrected interval of equilibrium
 202 sensitivities will be derived more simply and with less uncertainty than from the defective variant a_t ,
 203 and without the need to resort to GCMs (Monckton of Brenchley et al. 2015a). Terminology herein,
 204 though close to what is standard in control theory, may differ from the current climatological usage.

205 **Feedback** in any dynamical system (Fig. 2) responds to a **reference signal** $R_t > 0$ and modifies
 206 the **output signal** E_t . **Positive feedback** amplifies the output signal: **negative feedback** attenuates it.
 207 Reference and equilibrium temperatures R, E are time-dependent scalars. Since each may possess a
 208 unique value at a given time t , their subscript t indicates time-dependence.

209 It is generally assumed that feedbacks are time-invariant: the same input will yield similar outputs
 210 when applied at different points in time. However, where $E(R)$ is a nonlinear function the system-gain
 211 factor A may vary with different reference signals. Then A is a function of R , which is itself a function
 212 of time. Accordingly, the notation A_t is a shortened form of the notation $(A_R)_t$ for the system-gain
 213 factor corresponding to the specific value R_t of the reference temperature R at time t .



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 215 **FIG. 2.** The *feedback loop* (a) simplifies to (b), the schematic for the **system-gain factor** A_t at time t .
 216 The **reference signal** (**reference temperature** R_t), the sum of the **input signal** (**emission**
 217 **temperature** R_0), and all **perturbations** (**reference sensitivities** $\Delta R_0, \dots, \Delta R_{t-1}$), is input via the
 218 **summative input/output node** to the feedback loop. The **output signal** (**equilibrium temperature**
 219 E_t), is the sum of R_t and the **feedback response** $b_t := f_t E_t$ ($:= E_t - R_t$). Then A_t ($= E_t/R_t$) is equal
 220 to the sum $\sum_{i=0}^{\infty} f_t^i = (1 - f_t)^{-1}$ of the infinite convergent geometric series $\{f_t^0 + f_t^1 + \dots + f_t^{\infty}\}$
 221 under the convergence criterion $|f_t| < 1$. The **feedback block** (a) and the **system-gain block** (b) must
 222 perform act not only on the anthropogenic perturbation ΔR_{t-1} but on the entire reference signal R_t .

223 In climate, at time t , n **temperature feedback processes** $(\lambda_1)_t, (\lambda_2)_t, \dots, (\lambda_n)_t$, in Watts per
 224 square meter per Kelvin of the **reference temperature** R_t , sum to the **feedback sum** λ_t (Eq. 12).

$$\lambda_t = \sum_{i=1}^n (\lambda_i)_t. \quad (12)$$

225 The **feedback fraction** f_t of equilibrium sensitivity represented by the feedback response is the
 226 dimensionless product (Eq. 13) of λ_t and the Planck sensitivity parameter P_t , the latter in $\text{K W}^{-1} \text{m}^2$.

$$f_t = \lambda_t P_t. \quad (13)$$

227 **Mean emission flux density** Q_2 for total solar irradiance $S_0 = 1363.5 \text{ W m}^{-2}$ (Dewitte & Nevens
 228 2016, cf. Mekaoui et al. 2010) and mean planetary albedo $\alpha_2 = 0.3$ (Loeb 2009) is given by Eq. (14).

$$Q_2 = S_0(1 - \alpha_2)/4 = 238.6 \text{ W m}^{-2}. \quad (14)$$

229 The **Planck sensitivity parameter** P_2 is, to first approximation, the first derivative of the Stefan-
 230 Boltzmann equation. It may be taken (Schlesinger 1985) as the ratio (Eq. 15) of global mean surface
 231 temperature T_2 ($= 288.4 \text{ K}$ today: Morice et al. 2012) to four times the mean radiative flux density Q_2
 232 in Eq. (14). In today's climate, $P_2 \approx 0.30 \text{ K W}^{-1} \text{m}^2$ (based on Schlesinger 1985) or $0.31 \text{ K W}^{-1} \text{m}^2$
 233 (Soden & Held 2006; IPCC 2007, p. 631 fn.).

$$P_2 = T_2/4Q_2 = 288.4/(4 \times 238.6) \approx 0.30 \text{ K W}^{-1} \text{m}^2. \quad (15)$$

234 The reference signal before accounting for any temperature feedback is absolute global mean
 235 surface **reference temperature** R_t , the sum (in Eq. 16) of **emission temperature** R_0 in the absence of
 236 any NCGHGs and successive **reference sensitivities** $\Delta R_0, \Delta R_1, \dots, \Delta R_{t-1}$. In Fig. 2, the feedback block
 237 visibly acts not only upon one or more of the perturbations $\Delta R_0, \dots, \Delta R_{t-1}$ of R_0 , as is currently thought,
 238 but upon the entire reference signal R_t .

$$R_t := R_{t-1} + \Delta R_{t-1} := R_0 + \sum_{i=0}^{t-1} \Delta R_i. \quad (16)$$

239 Eq. (17) defines the **feedback response** b_t as the difference between **equilibrium temperature** E_t
 240 and **reference temperature** R_t , while Eq. (18) defines the **feedback fraction** f_t .

$$b_t := f_t E_t := E_t - R_t; \quad (17)$$

$$f_t = b_t / E_t = 1 - R_t / E_t. \quad (18)$$

241 Upon re-equilibration of the climate after accounting for the operation of the short-acting
 242 sensitivity-altering feedbacks (the term used in Bates 2016) represented by f_t , where **equilibrium**
 243 **sensitivity** is ΔE_{t-1} the output signal (Eq. 19) is absolute global mean surface **equilibrium**
 244 **temperature** E_t . *Ex definitione*, the **absolute system-gain factor** A_t that encompasses the entire action
 245 of feedback at time t is the ratio (in Eq. 20) of equilibrium to reference temperatures.

$$E_t = R_t + b_t := E_{t-1} + \Delta E_{t-1} \quad (19)$$

$$A_t = E_t / R_t = (R_t + f_t E_t) / R_t = (R_t + b_t) / R_t = (1 - f_t)^{-1}. \quad (20)$$

246 Feedback processes or their magnitudes may vary over time. Such feedbacks as are present at any
 247 specified time t must perforce respond to the entire reference signal then prevalent.

248 Linear algebra (Eq. 21) confirms the results in Eqs. (19, 20) and thus demonstrates Eq. (1):

$$\begin{aligned} & E_t := R_t + b_t := R_t + f_t E_t \\ \Rightarrow & R_t = E_t - b_t = E_t - f_t E_t = E_t(1 - f_t) \\ \Rightarrow & E_t = R_t / (1 - f_t) = R_t A_t \\ \Rightarrow & A_t = E_t / R_t = (1 - f_t)^{-1}. \end{aligned} \quad (21)$$

249 Since the signal transits the feedback loop infinitely, A_t is the sum of a convergent infinite
 250 geometric series whose common ratio at time t is the feedback fraction f_t . Eq. (22) gives the partial
 251 sum $(E_t)_n$ of the first n terms, for constant R_t . Then Eq. (23) is the product of Eq. (22) and f_t .

$$(E_t)_n = f_t^0 R_t + f_t^1 R_t + f_t^2 R_t + \dots + f_t^{n-1} R_t. \quad (22)$$

$$f_t (E_t)_n = f_t R_t + f_t^2 R_t + f_t^3 R_t + \dots + f_t^n R_t. \quad (23)$$

252 Since all but R_t in Eq. (22) and $f_t^n R_t$ in Eq. (23) cancel, Eq. (24) = Eq. (22) - Eq.(23):

$$\begin{aligned} (E_t)_n &= R_t + f_t R_t + f_t^2 R_t + f_t^3 R_t + \dots + f_t^{n-1} R_t \\ - [f_t (E_t)_n &= f_t R_t + f_t^2 R_t + f_t^3 R_t + \dots + f_t^{n-1} R_t + f_t^n R_t] \\ \hline = (1 - f_t)(E_t)_n &= R_t - f_t^n R_t = R_t(1 - f_t^n). \end{aligned} \quad (24)$$

253 The ratio of Eq. (24) and $(1 - f_t)$ is $(E_t)_n$ (Eq. 25), whereupon, under the convergence criterion
 254 $|f_t| < 1$, Eq. (26) follows.

$$(E_t)_n = R_t(1 - f_t^n)/(1 - f_t). \quad (25)$$

$$n \rightarrow \infty \Rightarrow (1 - f_t^n) \rightarrow 1 \Rightarrow R_t(1 - f_t^n) \rightarrow R_t. \quad (26)$$

255 Accordingly, for $|f_t| < 1$, in Eq. (27) E_t is the product of R_t and the convergent infinite
 256 geometric series $\{f_t^0 + f_t^1 \dots + f_t^\infty\}$, summing to $1/(1 - f_t)$, again demonstrating Eq. (1).

$$E_t = R_t \frac{1}{(1 - f_t)} = R_t + b_t = R_t + f_t E_t = R_t \sum_{i=1}^{\infty} f_t^i = R_t A_t \quad (27)$$

257 As is evident from Fig. 2, a feedback response occurs whenever a reference signal is present, and in
 258 response to that signal. With no reference signal, no feedback response arises. Accordingly, regardless
 259 of the shape of $E(R)$, $R_t = 0 \Rightarrow E_t = 0$, whereupon the point $(0, 0)$ always lies on the curve of $E(R)$.

260 4. The chief sensitivity-relevant feedbacks and the nonlinearities therein

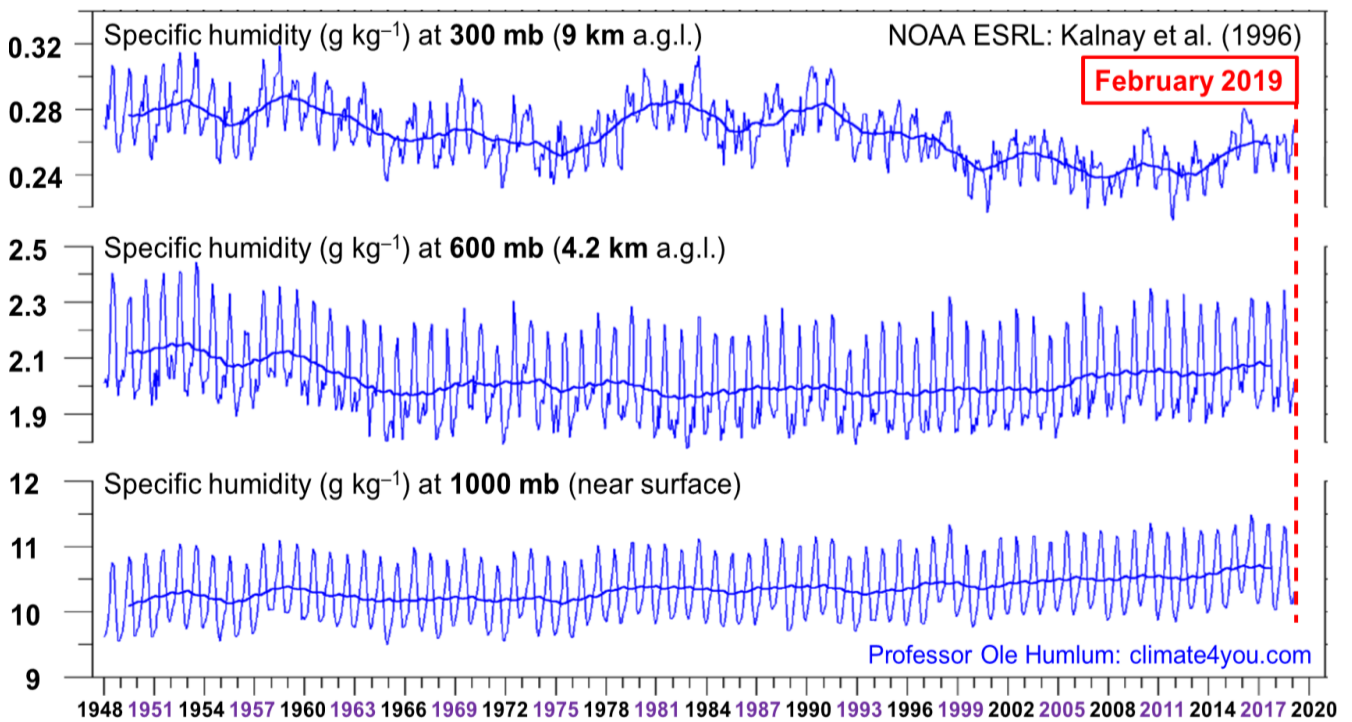
261 The principal sensitivity-relevant temperature feedbacks (Table 1) were no less applicable in the
 262 absence of the NCGHG than they are today. There are two important consequences. First, at any given
 263 time the great majority of the feedback response is attributable to emission temperature, which, in
 264 1850, represented some 92% of the equilibrium temperature then prevalent. Secondly, no large change
 265 in the feedback fraction f_t is to be expected over time. Charney sensitivity consequential upon IPCC's
 266 values for the sensitivity-relevant feedbacks in Table 1 is derived from their sum via the feedback
 267 fraction f_2 . IPCC's midrange estimates imply 2.6 K Charney sensitivity, almost 1 K below the 3.35 K
 268 midrange estimate implicit in results from the CMIP5 ensemble (Andrews et al. 2012). As will be seen,
 269 in reality Charney sensitivity is well below even 2.6 K. As Table 1 shows, in IPCC's understanding the
 270 midrange estimates of all sensitivity-relevant feedbacks other than water vapor effectively self-cancel.

271 **TABLE 1** Current feedbacks based on IPCC (2013, p. 818, table 9.5 and p. 128, Fig. 1.2)

Temperature feedback	Lower bound	Mid-range	Upper bound	Timescale
Water vapor feedback $(\lambda_1)_2$	+1.3 W m ⁻² K ⁻¹	+1.6 W m⁻² K⁻¹	+1.9 W m ⁻² K ⁻¹	Hours
Lapse rate feedback $(\lambda_2)_2$	-1.0 W m ⁻² K ⁻¹	-0.6 W m⁻² K⁻¹	-0.2 W m ⁻² K ⁻¹	Hours
Cloud feedback $(\lambda_3)_2$	-0.4 W m ⁻² K ⁻¹	+0.3 W m⁻² K⁻¹	+1.1 W m ⁻² K ⁻¹	Days
Surface albedo feedback $(\lambda_4)_2$	+0.2 W m ⁻² K ⁻¹	+0.3 W m⁻² K⁻¹	+0.4 W m ⁻² K ⁻¹	Years
IPCC feedback sum $\lambda_2 = \sum_{i=1}^4 (\lambda_i)_2$	+0.1 W m ⁻² K ⁻¹	+1.6 W m⁻² K⁻¹	+3.2 W m ⁻² K ⁻¹	Years
IPCC feedback fraction $f_2 = \lambda_2 P_2$	[+0.0]	+0.5	[+1.0]	
IPCC system-gain factor $a_2 = 1/(1 - f_2)$	[1.0]	2.0	[Undefined]	
IPCC implicit Charney sensi. $E_3 = \Delta R_2 a_2$	[1.0]	2.6	[∞]	

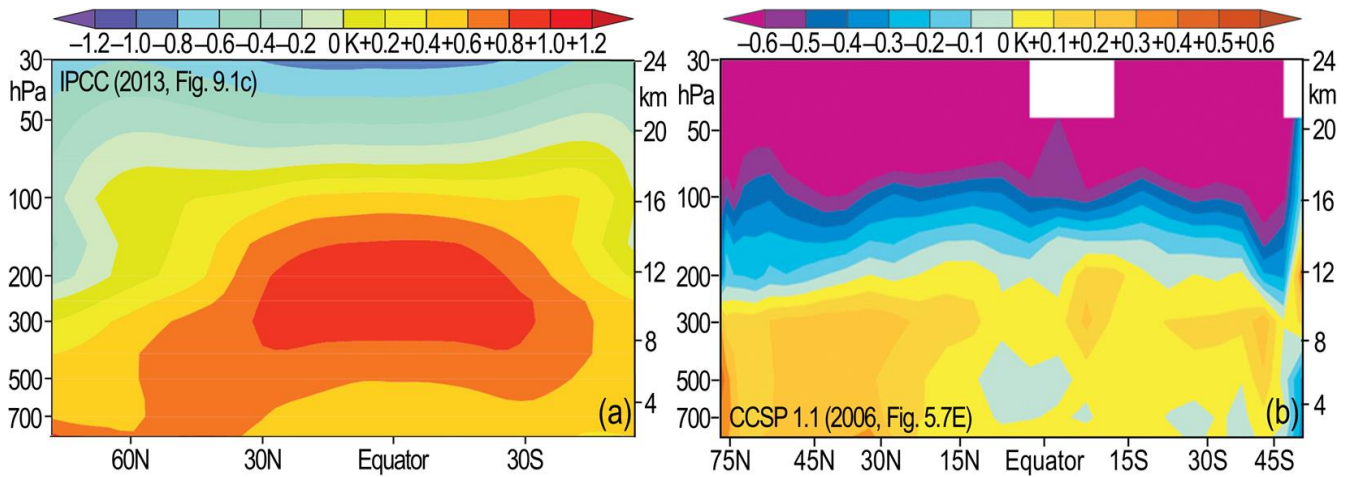
272 Some individual feedbacks $(\lambda_i)_2$ and hence λ_2, f_2, a_2 , vary nonlinearly with temperature. To
 273 address the question whether significant nonlinearities in feedback response may arise within a policy-
 274 relevant timeframe, each feedback in Table 1 is now considered, together with the Planck feedback.

275 **Water vapor and lapse-rate feedbacks:** Among the sensitivity-relevant feedbacks, column water
 276 vapor feedback predominates. In accordance with the Clausius-Clapeyron equation, specific humidity
 277 is expected to grow with warming by an observed $7\% \text{ K}^{-1}$ (Wentz et al. 2007). However, there are
 278 strong reasons to expect a modest feedback response to changes in specific humidity. As with CO_2 , so
 279 with water vapor, the forcing (here arising from feedback) is an approximately logarithmic function of
 280 the concentration. Furthermore, since ocean heat capacity is vast, negative feedbacks, such as the lapse-
 281 rate feedback and the earlier onset of tropical afternoon convection and cloud formation with warming,
 282 countervail to some degree against positive water-vapor feedback. In the lower troposphere, the only
 283 altitude at which specific humidity is rising as predicted (Kalnay et al. 1996, updated: Fig. 3), water
 284 vapor's spectral lines are near-saturated. Then, as specific humidity increases, only the far wings
 285 contribute to increased infrared absorption (Harde 2017). Absorption varies logarithmically with
 286 specific humidity: feedback response varies linearly with temperature.



287
 288 **FIG. 3** Specific humidity (g kg^{-1}) at 300, 600 and 1000 mb

289 In GCMs, some 90% of the water vapor feedback is projected to arise in the tropical mid-
 290 troposphere, where, however, specific humidity has been declining for several decades (Fig. 3). Perhaps
 291 for this reason, most datasets (e.g. those underlying Figs. 3, 4b) do not show the “hot spot” in the
 292 tropical mid-troposphere (Fig. 4a), where the GCMs (Fig. 4a) predict that warming will be twice the
 293 warming at the tropical surface. Douglass et al. (2008) were among the first to draw attention to this
 294 discrepancy, which Paltridge et al. (2009) attributed to subsidence drying of the upper and mid-
 295 troposphere. Without that differential rate of warming, the water vapor feedback cannot, as is currently
 296 thought, double the reference sensitivity. Overstated water vapor feedback is, therefore, likely to be the
 297 chief physical reason for the currently-overstated system-gain factor implicit in the GCMs.



298
299 **FIG. 4 GCMs' projected "hot spot"²⁸** (a) is absent in observational data¹¹ (b). Temperature
300 anomalies (in Kelvin) are color-coded.

301 Though Santer et al. (2008) attempted to reconcile the models' projections of the mid-troposphere
302 temperature profile with observations from 1979-1999, McKittrick et al. (2010) updated the datasets to
303 2009 and found that model-projected temperature trends in the lower as well as mid-troposphere
304 exceeded observation twofold to fourfold, reporting that the differences were statistically significant at
305 the 99% confidence interval. Christy (2010) noted that models projected that in the tropics the mid-
306 troposphere would warm 1.4 times faster than the surface, while observations showed the surface
307 warming 1.25 times faster than the mid-troposphere. While Thorne et al. (2011), in a meta-analysis,
308 found no compelling evidence of disagreement between models and observations, Fu et al. (2011)
309 found that the GCMs had overestimated the increase in static stability between the tropical mid- and
310 upper troposphere. Though Sherwood & Nishant (2015) reported "robust tropospheric warming" in the
311 tropics at a rate somewhat greater than at the surface, neither the RSS nor UAH satellite dataset shows
312 greater warming in the tropical mid-troposphere than at the tropical surface. The debate continues.

313 **Cloud feedback** is subject to substantial uncertainty, but the net effect of increased cloud cover on
314 temperature is one of cooling, in that the global shortwave cloud-albedo feedback exceeds the feedback
315 due to retention of longwave radiation by clouds (Ramanathan et al. 1989). Due to a reduction in cloud
316 cover, mean solar radiation at the Earth's surface increased by $0.16 \text{ W m}^{-2} \text{ yr}^{-1}$ from 1983-2001
317 (Pinker et al. 2005), accounting on its own for most of the global warming over the period (Monckton
318 of Brenchley 2011). From 2002 onward, the cloud cover reappeared, leading to a 15-year standstill in
319 global temperature. Since it is unlikely that a major change in global cloud cover will result from
320 increases in reference temperature, GCMs treat cloud feedback as small.

321 **Surface albedo feedback** responds chiefly to changes in northern-hemisphere snow cover, which,
322 however, has remained broadly constant during the period of satellite observation. For this reason, the
323 GCMs regard it as small. As for the cryosphere, since nearly all remaining ice is at very high latitudes
324 where the solar altitude is low, the contribution to surface albedo feedback from ice-melt is today
325 negligible, as the following analysis demonstrates.

326 Earth's surface area is $4\pi \times (6378.2 \text{ km})^2$, or 511 million km^2 . Minimum Arctic sea ice area is 4
327 million km^2 , or 0.8% of the Earth's surface. Ice albedo is 0.66 (Pierrehumbert 2011). Assuming
328 ocean-water albedo 0.06 if all the Arctic ice were to melt for the late-summer quarter, global mean
329 albedo, now 0.3, would become $0.3 - 0.008 (0.66 - 0.06)$, or 0.295. However, high-Arctic insolation
330 is only one-quarter as powerful as mean terrestrial insolation, requiring division by 4; summer ice loss
331 endures for at most 3 months, or half of the Arctic daylight period, requiring division by 2; and the
332 Arctic has 75% cloud cover, requiring a further division by 4. Thus, Eq. (28) gives the revised global
333 mean present-day albedo α_2 assuming total Arctic ice-melt in the late-summer quarter, which proves to
334 be vanishingly different from today's albedo.

$$\alpha_2 = 0.3 - 0.008 \frac{0.66 - 0.06}{4 \times 2 \times 4} = 0.2999. \quad (28)$$

335 The difference ΔR_0 in current emission temperature (Eq. 29), and in surface temperature ΔT_0 from
336 the near-linear lapse rate, for TSI $S_0 = 1363.5 \text{ W m}^{-2}$ and the Stefan-Boltzmann constant σ , is:

$$\Delta T_0 = \Delta R_0 = [S_0(1 - 0.3)/4\sigma]^{1/4} - [S_0(1 - 0.2999)/4\sigma]^{1/4} = 0.009 \text{ K}. \quad (29)$$

337 This first-order analysis indicates that, even if the entire Arctic icecap were to melt for three
338 months every summer, very little change in surface albedo feedback would arise. Therefore, even if
339 that feedback were nonlinear, it is and, in foreseeable modern conditions, will remain too small to be
340 significant. This conclusion is consistent with the findings of two recent evaluations of snow-cover
341 feedbacks in current climate models: Rosenblum & Eisenman (2017) and Connolly et al. (2019).

342 **Planck feedback**, not separately listed by IPCC and not shown in Table 1, is likewise *de minimis*.
343 Assuming constant insolation at 1363.5 W m^{-2} and constant albedo at 0.3, giving mean emission-
344 altitude flux density of 238.6 W m^{-2} , and assuming equilibrium temperature $E_1 = 287.55 \text{ K}$ in 1850,
345 the Planck parameter P_1 was $287.55/(4 \times 238.6) = 0.301$; for 2011, P_2 was $288.5/954.4 = 0.302$; at
346 $2\times\text{CO}_2$ it would be $(288.5 + 3.35)/954.4 = 0.306$. The three ratios are near-identical. Here, too, the
347 change over time is small.

348 Since significant nonlinearities in the response to any individual temperature feedback are not to be
349 expected, the feedback regime is likely to be approximately linear and time-invariant. Nevertheless,
350 various exponential-growth scenarios will now be studied and their plausibility assessed.

351 **5. Evolution of the equilibrium-sensitivity function $E(R)$**

352 At each successive time t at which radiative equilibrium prevails, there subsists a distinct absolute
353 value of the system-gain factor A_t reflecting the entire feedback response b_t to reference sensitivity R_t
354 and the consequent modification of equilibrium sensitivity E_t by the feedback processes then prevalent.
355 Four illustrative equilibria in the evolution of climate will be studied:

$t = 0$ at emission temperature R_0 , before accounting for any forcing or feedback;
 $t = 1$ in 1850, the date at which IPCC currently takes the industrial era as commencing;
 $t = 2$ in 2011, the date to which climate-relevant data were updated for IPCC (2013); and
 $t = 3$ upon a radiative forcing equivalent to a CO₂ doubling compared with 2011.

Direct perturbations in the concentration of the NCGHGs (chiefly CO₂, CH₄, O₃ and N₂O) are treated as radiative forcings, while consequential forcings arising from perturbations in the burden of the condensing greenhouse gas water vapor are counted among the temperature feedbacks. Such NCGHG feedbacks, including the CO₂ feedback, are overlooked here. They are subject to very large uncertainty. IPCC (2013, p. 818, table 9.5) omits them from its list of sensitivity-relevant feedbacks (Table 1).

As a first step, values of R_t will be derived as the basis for deriving E_t under various evolutionary scenarios. Here and throughout, temperatures will be given to the nearest 0.05 K.

For $t = 0$, emission temperature R_0 is the starting-point. Given present-day total solar irradiance S_0 ($= 1363.50 \text{ W m}^{-2}$), mean planetary albedo $\alpha = 0.31$ (Soden & Held 2006; *cf.* Loeb 2009) and the Stefan-Boltzmann constant $\sigma = 5.6704 \times 10^{-8} \text{ W m}^{-2} \text{ K}^{-4}$, R_0 is given by Eq. (30).

$$R_0 = [S_0(1 - \alpha)/(4\sigma)]^{1/4} = 254.70 \text{ K} \quad (30)$$

With no greenhouse gases and before allowing for feedback, R_0 would prevail at the Earth's surface. With NCGHG-driven warming as well as feedback processes such as the water vapor feedback, the effective emission altitude has risen and is now in the mid-troposphere. Climatology does not currently make allowance for Hölder's inequalities in deriving R_0 : that question will be addressed later.

For $t = 1$ in 1850, the point (R_1, E_1) is well constrained, providing a datum for all the scenarios that follow. Equilibrium temperature E_1 was 287.55 K that year. Implicit reference sensitivity ΔR_0 to the NCGHGs was $0.25(287.55 - 252 \text{ K}) = 8.90 \text{ K}$ (Lacis et al. 2010). Alternatively, the anthropogenic CO₂ forcing of 1.68 W m^{-2} from 1850-2011 represented 75% of the 2.49 W m^{-2} net period anthropogenic radiative forcing (the midrange 2.29 W m^{-2} in IPCC 2013, fig. SPM.5, with 0.2 W m^{-2} added to correct IPCC's overstatement of the negative aerosol forcing). Then, for a 30 W m^{-2} total CO₂ forcing to date (Schmidt et al. 2010), anthropogenic forcing ΔQ_0 was $(30 - 1.68)/0.75$, or 37.76 W m^{-2} . Reference sensitivity $\Delta R_0 = \Delta Q_0 P_1$ was thus $37.76 \times 0.31 = 11.7 \text{ K}$. A fair midrange estimate of ΔR_0 is the mean of these two estimates: i.e., $(8.9 + 11.7)/2$, or 10.30 K . Then reference temperature R_1 , the sum of emission temperature R_0 and reference sensitivity ΔR_0 to the pre-industrial NCGHGs, was 265 K in 1850. In the presence of the pre-industrial NCGHGs, equilibrium temperature E_1 ($= 287.55 \text{ K}$) was the difference between today's global mean surface temperature T_S ($= 288.4 \text{ K}$; Morice et al. 2012) and the 0.85 K least-squares linear-regression trend on the HadCRUT4 data from 1850-2018. The climate was approximately at equilibrium in 1850: there was to be no trend in global temperature for 80 years. Since uncertainties in R_1, E_1 are quite small, and since anthropogenic perturbation had had little effect by 1850, A_1 ($= E_1/R_1$) was equal to 1.085 in that year.

390 **For $t = 2$** in 2011, net midrange anthropogenic radiative forcing ΔQ_1 is given as 2.29 W m^{-2}
 391 (IPCC 2013, fig. SPM.5); but many authors (e.g. Seifert et al. 2015; Stevens 2015; Fiedler et al. 2017;
 392 Sato et al. 2018) find the aerosol forcing less negative than IPCC (2013). Applying a 0.2 W m^{-2}
 393 adjustment (Armour 2017: for a discussion, see Lewis & Curry 2018), the midrange estimate of ΔQ_1
 394 rises to 2.49 W m^{-2} . Thus, ΔR_1 , the product of ΔQ_1 and the Planck parameter $P_2 = 0.31 \text{ K W}^{-1} \text{ m}^2$,
 395 was 0.75 K in 2011, so that reference temperature R_2 , the sum of R_1 and ΔR_1 , was 265.75 K .

396 **For $t = 3$** following a radiative forcing $\Delta Q_2 = 3.45 \text{ W m}^{-2}$ equivalent to the forcing from
 397 doubled CO_2 (half of the mean of the $4\times\text{CO}_2$ forcings found in 15 CMIP5 models listed in Andrews 2012,
 398 table 1), $\Delta R_2 = P_2 \Delta Q_2 = 1.05 \text{ K}$. Then reference temperature R_3 , the sum of R_2 and ΔR_2 , would be
 399 266.80 K . Since the mean midrange Charney sensitivity $(\Delta E_2)_M$ in the same models (*ibid.*) was 3.35 K ,
 400 the models' midrange system-gain factor $(A_M)_3$ implicit in the CMIP5 outputs is $(\Delta E_M)_2/\Delta R_2$, or 3.2 .

401 Table 2 summarizes the evolution of reference temperature R_t .

402 **TABLE 2** Evolution of midrange reference temperature R_t (to the nearest 0.05 K).

Emission temperature	Pre-industrial	In 1850	1850-2011	In 2011	2011- $2\times\text{CO}_2$	At $2\times\text{CO}_2$
R_0	ΔR_0	R_1	ΔR_1	R_2	ΔR_2	R_3
254.70 K	10.30 K	265.00 K	0.75 K	265.75 K	1.05 K	266.80 K

403 **6. Five models of the equilibrium-sensitivity response function $E(R)$**

404 Since the shape of $E(R)$ is not known, values of $R, \Delta R$ in Table 2 will be deployed in five illustrative
 405 evolutions consistent with empirical data; four exponential-growth models and a linear-growth model.
 406 It will become apparent that current climate-sensitivity estimates are excessive, since they imply a
 407 disproportionately large feedback fraction in response to both natural and anthropogenic greenhouse
 408 warming compared with the feedback fraction in response to emission temperature. Model 1 assumes
 409 that current midrange Charney-sensitivity estimates are correct. Model 2 assumes that the feedback
 410 response grows at 7% per Kelvin of reference temperature. Model 3 assumes that the current
 411 observationally-based implicit midrange estimate of the anthropogenically-forced warming from 1850-
 412 2011 is correct. Model 4 assumes that a zero temperature implies a zero feedback response. Model 5 is
 413 a linear-growth model.

414 **Model 1** is derived from current midrange Charney-sensitivity estimates. $E(R)$ is taken as an
 415 exponential-growth function derived from points $(R_1, E_1), (R_3, E_3)$, where R_1, R_3 are as in Table 2,
 416 $E_1 = 287.55 \text{ K}$ and E_3 is derived from the CMIP5 system-gain factor $(A_M)_3$ via Eq. (31).

$$E_3 = E_1 + (A_M)_3(\Delta R_1 + \Delta R_2) = 293.30 \text{ K.} \quad (31)$$

417 The shape of a unique exponential-growth function is derivable from any two specified points on
 418 the curve of the function. Here, on an exponential curve $E_t = k_1 \exp(k_2 R_t)$, the constants k_1, k_2 of
 419 exponentiality are derived from points $(R_1, E_1), (R_3, E_3)$. Solving the simultaneous equations (32, 33)

420 by way of Eqs. (34, 35) yields the constants k_1, k_2 (Eqs. 36, 37). Then the point-slope s_t at any point
 421 (R_t, E_t) is the first derivative (Eq. 38) of the function at that point, while Eq. (39) gives the slope a_t of
 422 the secant between points $(R_{t-1}, E_{t-1}), (R_t, E_t)$.

$$E_1 = k_1 \exp(k_2 R_1); \quad (32)$$

$$E_3 = k_1 \exp(k_2 R_3). \quad (33)$$

$$E_1/E_3 = \exp(k_2 R_1 - k_2 R_3) = \exp[k_2(R_1 - R_3)] \quad (34)$$

$$\ln(E_1/E_3) = k_2(R_1 - R_3) \quad (35)$$

$$k_2 = \ln(E_1/E_3)/(R_1 - R_3) = 0.0110; \quad (36)$$

$$k_1 = E_1 \exp(-k_2 R_1) = 15.4883. \quad (37)$$

$$s_t = k_1 k_2 \exp(k_2 R_t); \quad (38)$$

$$a_t = (E_t - E_{t-1})/(R_t - R_{t-1}) \quad (39)$$

423 Table 3 gives reference temperatures R_t , equilibrium temperatures E_t , feedback responses b_t ,
 424 feedback fractions f_t , system-gain factors A_t , point-slopes s_t and secant-slopes a_t for model 1.

425 **TABLE 3** Results from model 1

Emiss. temp.	Pre-industrial	In 1850	1850-2011	In 2011	2011 to 2xCO ₂	At 2xCO ₂
R_0 254.70 K	ΔR_0 10.30 K	R_1 265.00 K	ΔR_1 0.75 K	R_2 265.75 K	ΔR_2 1.05 K	R_3 266.80 K
E_0 256.70 K	ΔE_0 30.85 K	E_1 287.55 K	ΔE_1 2.40 K	E_2 289.95 K	ΔE_2 3.40 K	E_3 293.30 K
b_0 2.00 K	Δb_0 20.55 K	b_1 22.55 K	Δb_1 1.65 K	b_2 24.20 K	Δb_2 2.35 K	b_3 26.50 K
f_0 0.0078	Δf_0 0.6663	f_1 0.0784	Δf_1 0.6858	f_2 0.0834	Δf_2 0.6889	f_3 0.0904
A_0 1.0078	ΔA_0 2.9966	A_1 1.0851	ΔA_1 3.1831	A_2 1.0910	ΔA_2 3.2149	A_3 1.0994
s_0 2.8297	(a_0) (2.9966)	s_1 3.1700	(a_1) (3.1831)	s_2 3.1963	(a_2) (3.2149)	s_3 3.2335

426 At $t = 0$, the feedback response b_0 to the 254.70 K emission temperature R_0 is only 2.00 K, so
 427 that equilibrium temperature E_0 before accounting for any NCGHGs is 256.70 K and the feedback
 428 fraction $f_0 (= b_0/E_0)$ is just 0.0078. However, the feedback response Δb_0 to the 10.30 K reference
 429 sensitivity ΔR_0 driven by warming from the pre-industrial NCGHGs is 20.55 K. The feedback fraction
 430 $\Delta f_0 (= \Delta b_0/\Delta R_0)$ is 0.6663, exceeding f_0 by two orders of magnitude. Any such outcome is in
 431 practice impossible: there is no legitimate theoretical or empirical reason to suppose that the presence
 432 of the NCGHGs altered the pre-existing feedback regime so drastically as to increase the feedback
 433 fraction 85-fold. Therefore, an exponential-growth model dependent upon the assumption that anything
 434 like the current projections of Charney sensitivity are correct is untenable.

435 Another significant conclusion from this experiment is that the feedback fraction cannot approach
 436 unity, as is currently thought (see e.g. Schlesinger 1985; Roe, 2009). Once it is appreciated that
 437 feedback responds not only to perturbations but also to emission temperature, the notion of a “tipping-
 438 point” beyond which runaway feedbacks may rapidly and uncontrollably drive up global temperature
 439 becomes insupportable.

440 **Model 2** assumes that the feedback response b_t , dependent chiefly upon the water-vapor feedback,
 441 will grow exponentially at 7% per Kelvin of reference temperature R_t in line with the currently-

442 projected 7% K⁻¹ Clausius-Clapeyron growth in specific humidity with temperature (Wentz et al.
 443 2007). In reality, there is an approximately logarithmic relation between change in specific humidity
 444 and change in water-vapor feedback forcing, implying an approximately linear temperature response to
 445 the water-vapor feedback. Nevertheless, model 2 takes $E(R)$ as an exponential-growth function derived
 446 from points (R_1, E_1) , (R_3, E_3) , where R_1, R_3 are as in Table 2; E_1 is the observed global mean surface
 447 temperature in 1850; and E_3 is the sum of R_3 and b_3 as derived in Eq. (40).

$$E_3 = R_3 + b_3 = R_3 + b_1(1.07^{\Delta R_1 + \Delta R_2}) = 266.80 + 25.50 = 292.25 \text{ K.} \quad (40)$$

448 Calculation proceeds as in model 1. Eqs. (41, 42) give the constants k_1, k_2 of exponentiality.

$$k_2 = \ln(E_1/E_3)/(R_1 - R_3) = 0.0090; \quad (41)$$

$$k_1 = E_1 \exp(-k_2 R_1) = 26.1495. \quad (42)$$

449 Table 4 gives reference temperatures R_t , equilibrium temperatures E_t , feedback responses b_t ,
 450 feedback fractions f_t , system-gain factors A_t , point-slopes s_t and secant-slopes a_t for model 2.

451 **TABLE 4** Results from model 2

Emiss. temp.	Pre-industrial	In 1850	1850-2011	In 2011	2011 to 2xCO ₂	At 2xCO ₂
R_0 254.70 K	ΔR_0 10.30 K	R_1 265.00 K	ΔR_1 0.75 K	R_2 265.75 K	ΔR_2 1.05 K	R_3 266.80 K
E_0 261.95 K	ΔE_0 25.60 K	E_1 287.55 K	ΔE_1 1.95 K	E_2 289.50 K	ΔE_2 2.75 K	E_3 292.25 K
b_0 7.25 K	Δb_0 15.30 K	b_1 22.55 K	Δb_1 1.20 K	b_2 23.75 K	Δb_2 1.70 K	b_3 25.50 K
f_0 0.0277	Δf_0 0.5974	f_1 0.0784	Δf_1 0.6169	f_2 0.0821	Δf_2 0.6200	f_3 0.0872
A_0 1.0285	ΔA_0 2.4841	A_1 1.0851	ΔA_1 2.6105	A_2 1.0894	ΔA_2 2.6318	A_3 1.0955
s_0 2.3701	(a_0) (2.4841)	s_1 2.6016	(a_1) (2.6105)	s_2 2.6194	(a_2) (2.6318)	s_3 2.6444

452 As with model 1, model 2 is in practice impossible. The feedback response to the 254.7 K emission
 453 temperature is only 7.25 K; yet the feedback response to the 10.3 K sensitivity to the pre-industrial
 454 NCGHGs is 15.3 K. The feedback fraction Δf_0 in response to the pre-industrial NCGHGs exceeds the
 455 feedback fraction f_0 in response to emission temperature 22-fold. Once again, there is no plausible
 456 physical explanation for any such sudden increase in the feedback fraction.

457 **Model 3** represents an exponential growth function $E(R)$ derived both from the well-constrained
 458 reference and equilibrium temperatures at point (R_1, E_1) in 1850 and from the current midrange
 459 projected values of those temperatures at point (R_2, E_2) in 2011, derived from the projected net
 460 anthropogenic forcing from 1850-2011 in IPCC (2013, fig. SPM.5). Since the climate was not in
 461 radiative equilibrium in 2011, the 0.75 K observed warming from 1850-2011 was not an equilibrium
 462 sensitivity; and the anthropogenic fraction of observed warming is unknown (Legates et al., 2015). To
 463 overcome these difficulties, an energy-balance model (Gregory 2004, Lewis & Curry 2018) was used.

464 To derive the temperature E_2 that would have prevailed if the climate had been in radiative
 465 equilibrium in 2011, one must allow for the change ΔN_{t-1} in the estimated top-of-atmosphere net
 466 radiative imbalance N_t at time $t = 2$ in 2011, assuming that the change Δq_{t-1} in net outgoing radiation
 467 consequent upon the net anthropogenic radiative forcing ΔQ_{t-1} is linearly proportional to reference

468 sensitivity ΔR_{t-1} . In Eq. (43), the temperature-feedback parameter $(\lambda_F)_t$ is the growth in the net
 469 outgoing radiative flux Δq_{t-1} per Kelvin of surface warming ΔR_{t-1} . Internal variability is ignored. By
 470 conservation of energy, Eq. (44) gives the radiative imbalance ΔN_{t-1} . Then the feedback parameter
 471 $(\lambda_F)_t$, derived from Eqs. (43, 44), is given by Eq. (45).

$$(\lambda_F)_t = \Delta q_{t-1} / \Delta R_{t-1}. \quad (43)$$

$$\Delta N_{t-1} = \Delta Q_{t-1} - \Delta q_{t-1}. \quad (44)$$

$$(\lambda_F)_t = (\Delta Q_{t-1} - \Delta N_{t-1}) / \Delta R_{t-1}. \quad (45)$$

472 Where ΔQ_{t-1} is the radiative forcing and ΔE_{t-1} is equilibrium sensitivity, once the climate system
 473 has settled to equilibrium (i.e., where $\Delta N_{t-1} = 0$), Eq. (46) yields the temperature feedback parameter
 474 $(\lambda_F)_t$, whereupon, by substitution in Eq. (45), Eq. (47) yields equilibrium sensitivity ΔE_{t-1} . Since
 475 reference sensitivity ΔR_{t-1} is the product of the Planck sensitivity parameter P_t and the forcing ΔQ_{t-1} ,
 476 Eq. (47) is recast as Eq. (48) to give the slope a_1 of the secant from 1850-2011. It is this slope that
 477 climatology takes to be its system-gain factor.

$$(\lambda_F)_t = \Delta Q_{t-1} / \Delta E_{t-1}, \quad (46)$$

$$\Delta E_{t-1} = \Delta Q_{t-1} \frac{\Delta R_{t-1}}{\Delta Q_{t-1} - \Delta N_{t-1}}. \quad (47)$$

$$a_1 = \frac{E_2 - E_1}{R_2 - R_1} = \frac{\Delta E_1}{\Delta R_1} = \frac{\Delta E_1}{\Delta Q_1 P_2} = \frac{\Delta Q_1}{\Delta Q_1 - \Delta N_1}. \quad (48)$$

478 Anthropogenic forcing ΔQ_1 from 1850-2011 and radiative imbalance ΔN_1 to 2010 are subject to
 479 large uncertainties. Midrange estimates are $\Delta Q_1 = 2.49 \text{ W m}^{-2}$ (2.29 W m^{-2} IPCC 2013, fig. SPM.5,
 480 adjusted for a 0.2 W m^{-2} overestimate of negative aerosol forcing, based on Armour 2017), and $\Delta N_1 =$
 481 0.6 W m^{-2} (Smith et al. 2015). Then the midrange estimate of the slope a_1 of the industrial-era secant
 482 from 1850-2011 (Eq. 48) is 1.3175, implying period equilibrium sensitivity $\Delta E_1 = 1.0 \text{ K}$, so that
 483 equilibrium temperature $E_2 (= E_1 + \Delta E_1)$ was 288.55 K. However, the true system-gain factor $A_2 (=$
 484 $E_2/R_2 = 288.55/265.75)$ was 1.086, scarcely above $A_1 = 1.085$. Here, $k_1 = 0.0045$ and $k_2 =$
 485 85.5720. Table 5 gives results for model 3.

486 **TABLE 5** Results from model 3

Emiss. temp.	Pre-industrial	In 1850	1850-2011	In 2011	2011 to 2xCO ₂	At 2xCO ₂
R_0 254.70 K	ΔR_0 10.30 K	R_1 265.00 K	ΔR_1 0.75 K	R_2 265.75 K	ΔR_2 1.05 K	R_3 266.80 K
E_0 274.30 K	ΔE_0 13.25 K	E_1 287.55 K	ΔE_1 1.00 K	E_2 288.55 K	ΔE_2 1.40 K	E_3 289.95 K
b_0 19.60 K	Δb_0 2.95 K	b_1 22.55 K	Δb_1 0.25 K	b_2 22.80 K	Δb_2 0.35 K	b_3 23.15 K
f_0 0.0715	Δf_0 0.2216	f_1 0.0784	Δf_1 0.2410	f_2 0.0790	Δf_2 0.2441	f_3 0.0798
A_0 1.0770	ΔA_0 1.2847	A_1 1.0851	ΔA_1 1.3175	A_2 1.0858	ΔA_2 1.3229	A_3 1.0867
s_0 1.2547	(a_0) (1.2847)	s_1 1.3152	(a_1) (1.3175)	s_2 1.3197	(a_2) (1.3229)	s_3 1.3261

487 Model 3 is less implausible than models 1-2, showing feedback responses of 19.6 K to the
 488 254.70 K emission temperature, and of 2.95 K to the 10.3 K reference sensitivity to the pre-industrial
 489 NCGHG. However, the feedback fractions are 0.0715 and 0.2216 respectively: even here, implausibly,

490 the feedback fraction in response to the NCGHG is thrice that in response to emission temperature.
 491 Model 3 also suggests that, on the basis of the 1.05 K industrial-era equilibrium sensitivity, Charney
 492 sensitivity would be only 1.4 K, not the CMIP5 models' currently-projected 3.35 K.

493 **Model 4** correctly takes a zero temperature as entailing no feedback response; the y-intersect is 0.
 494 For an exponential-growth curve $E = R^x$ through points (0,0), $(R_1, E_1) = (265.00, 287.55)$, Eq. (49)
 495 gives the exponent x , whereupon Eq. (50) gives E_t for any value of R_t .

$$x = \ln(E_1/R_1) = 1.0146. \quad (49)$$

$$E_t = R_t^x. \quad (50)$$

496 Table 6 gives results for model 4.

497 **TABLE 6** Results from model 4

Emiss. temp.	Pre-industrial	In 1850	1850-2011	In 2011	2011 to 2xCO ₂	At 2xCO ₂
R_0 254.70 K	ΔR_0 10.30 K	R_1 265.00 K	ΔR_1 0.75 K	R_2 265.75 K	ΔR_2 1.05 K	R_3 266.80 K
E_0 276.20 K	ΔE_0 11.35 K	E_1 287.55 K	ΔE_1 0.85 K	E_2 288.40 K	ΔE_2 1.15 K	E_3 289.55 K
b_0 21.50 K	Δb_0 1.05 K	b_1 22.55 K	Δb_1 0.10 K	b_2 22.65 K	Δb_2 0.10 K	b_3 22.75 K
f_0 0.0779	Δf_0 0.0915	f_1 0.0784	Δf_1 0.0918	f_2 0.0785	Δf_2 0.0918	f_3 0.0785
A_0 1.0845	ΔA_0 1.1007	A_1 1.0851	ΔA_1 1.1010	A_2 1.0852	ΔA_2 1.1011	A_3 1.0852
s_0 1.1004	(a_0) (1.1007)	s_1 1.1010	(a_1) (1.1010)	s_2 1.1010	(a_2) (1.1011)	s_3 1.1011

498 Since the exponent x , calculated from the two reliable points (0,0) and (265.00, 287.55), is only
 499 1.0146 (Eq. 49), model 4 is very close to linear. It is a plausible model, since the feedback fraction in
 500 response to the pre-industrial NCGHGs, at 0.0915, exceeds the feedback fraction 0.0779 in response to
 501 emission temperature by little more than one-sixth, which is not impossible.

502 **Model 5** takes $E(R)$ as a linear function whose slope is equal to A_1 ($= E_1/R_1 = 1.085$). Results
 503 for model 5 are almost identical to those for model 4, since the exponential-growth curve in model 4 is
 504 very close to linear. For this reason, it is legitimate to obtain approximate estimates of Charney
 505 sensitivity using an assumption of linearity in feedback response. Charney sensitivity in model 5, as in
 506 model 4, is 1.15 K. Table 7 gives results for model 5.

507 **TABLE 7** Results from model 5

Emiss. temp.	Pre-industrial	In 1850	1850-2011	In 2011	2011 to 2xCO ₂	At 2xCO ₂
R_0 254.70 K	ΔR_0 10.30 K	R_1 265.00 K	ΔR_1 0.75 K	R_2 265.75 K	ΔR_2 1.05 K	R_3 266.80 K
E_0 276.35 K	ΔE_0 11.20 K	E_1 287.55 K	ΔE_1 0.80 K	E_2 288.35 K	ΔE_2 1.15 K	E_3 289.50 K
b_0 21.70 K	Δb_0 0.90 K	b_1 22.55 K	Δb_1 0.05 K	b_2 22.60 K	Δb_2 0.10 K	b_3 22.70 K
f_0 0.0784	Δf_0 0.0784	f_1 0.0784	Δf_1 0.0784	f_2 0.0784	Δf_2 0.0784	f_3 0.0784
A_0 1.0851	ΔA_0 1.0851	A_1 1.0851	ΔA_1 1.0851	A_2 1.0851	ΔA_2 1.0851	A_3 1.0851
s_0 1.0851	(a_0) (1.0851)	s_1 1.0851	(a_1) (1.0851)	s_2 1.0851	(a_2) (1.0851)	s_3 1.0851

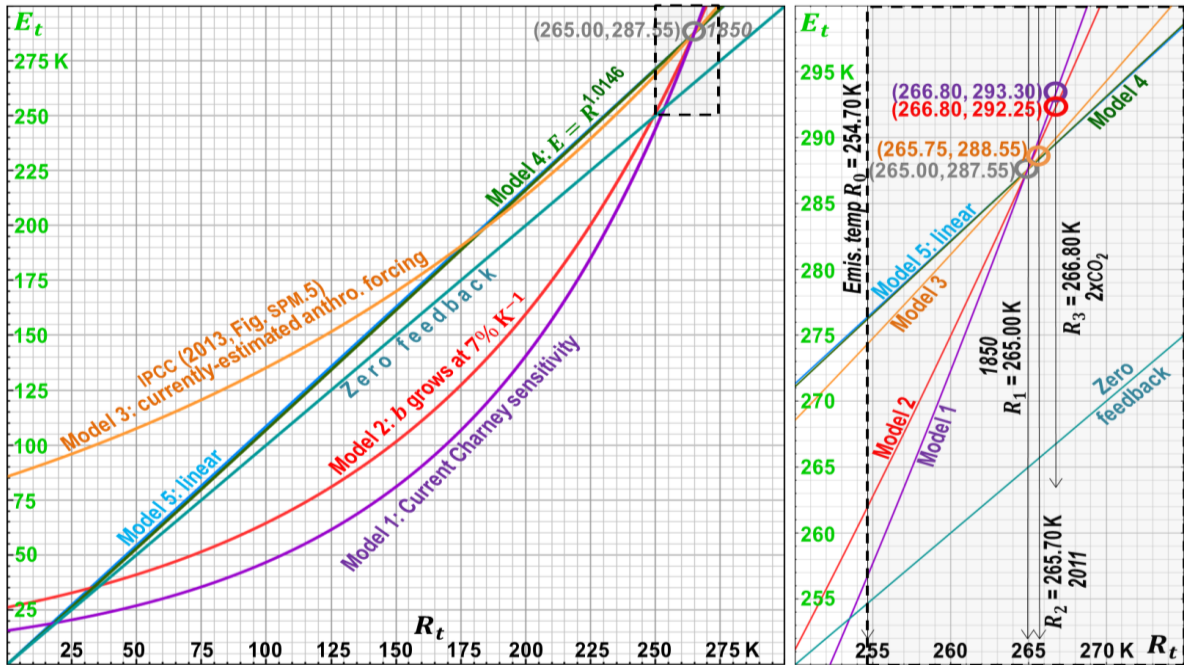
508 Which model is preferable? Models 4, 5 have many advantages. Not the least of these is that, as
 509 expected, $R_t = 0 \Rightarrow E_t = 0$. All the other models imply, *per impossibile*, that a zero temperature will
 510 drive a positive feedback response. However, the chief advantage of models 4, 5 is that they take full
 511 account of the fact that feedback processes respond not only to anthropogenic perturbations in emission

512 temperature but also to natural perturbations and also, most importantly, to emission temperature itself.
 513 The feedback response to emission temperature is, as it should be, larger than the feedback response to
 514 the pre-industrial NCGHG-driven warming, which is in turn larger than the feedback response to the
 515 smaller anthropogenic perturbation after 1850.

516 For comparison between the five models, Table 8 gives feedback responses $b_0, \Delta b_0$, feedback
 517 fractions $f_0, \Delta f_0$, feedback-fraction ratios $\Delta f_0/f_0$, system-gain factors A_3 and Charney sensitivities ΔE_2 .

518 **TABLE 8** Relationship between elevated ratios $\Delta f_0/f_0$ and elevated Charney sensitivities ΔE_2

Model	b_0	Δb_0	f_0	Δf_0	$\Delta f_0/f_0$	A_3	ΔE_2
CMIP5 current ΔE_2 : 1	2.00 K	20.55 K	0.0078	0.6663	85	1.0994	3.40 K
$b_t + 1.07\% K^{-1}$: 2	7.25 K	15.30 K	0.0277	0.5974	22	1.0955	2.75 K
IPCC anth. forcing: 3	19.60 K	2.95 K	0.0715	0.2216	3.1	1.0867	1.40 K
$R = 0 \Rightarrow b = 0$: 4	21.50 K	1.05 K	0.0779	0.0915	1.2	1.0852	1.15 K
Linear: 5	21.70 K	0.90 K	0.0784	0.0784	1.0	1.0851	1.15 K

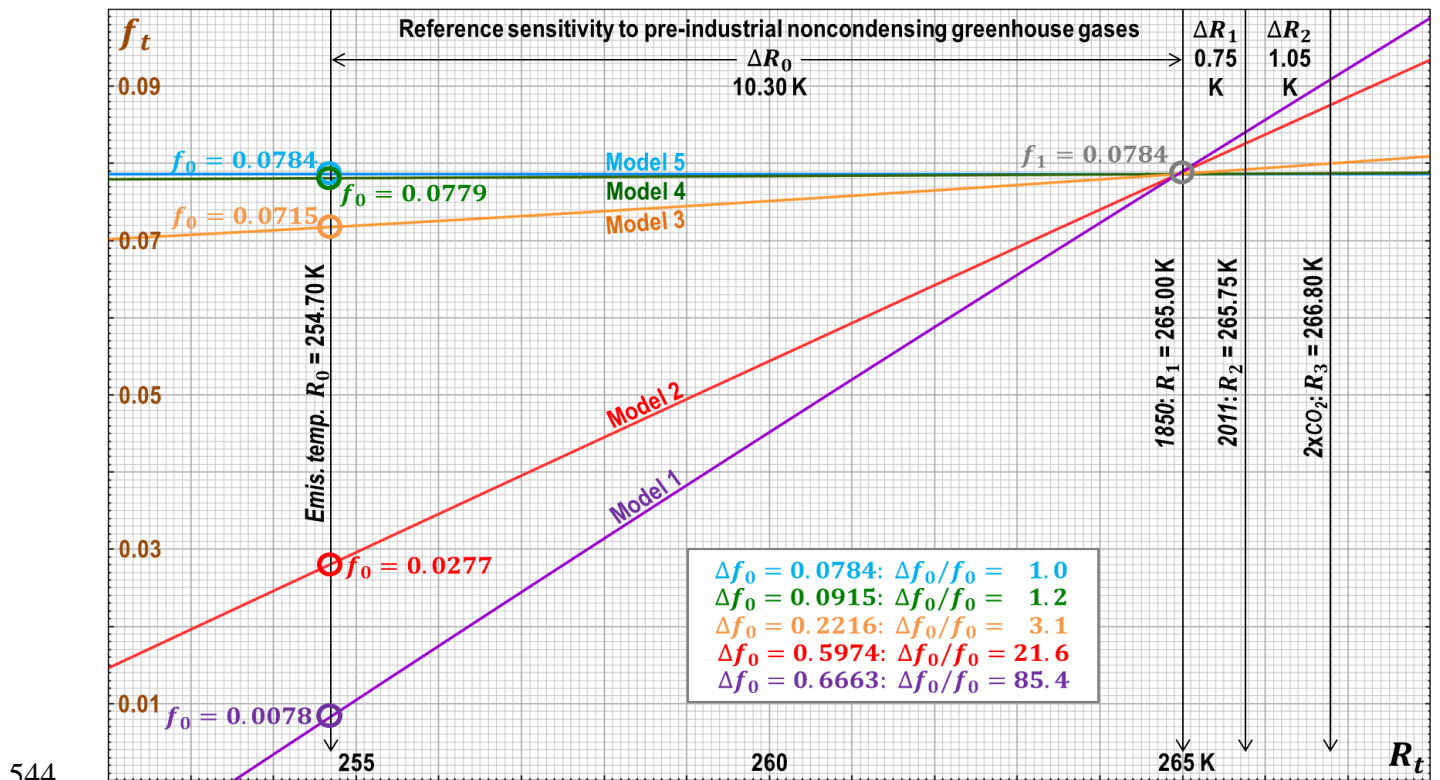


519 **FIG. 5** Comparison of the five models of the evolution of $E(R)$ for R on $[250, 275]$ K.
 520 Models 1 (purple), 2 (red) and 3 (orange) are each generated from two points: the circled
 521 points in their colors and the common gray point $(265.00, 287.55)$ representing the
 522 position in 1850. In model 4 (green), the exponent $x = \ln(287.55)/\ln(265.70) = 1.0146$.
 523 Model 5 (pale blue) is the linear model. For comparison, the zero-feedback line $E = R$ is
 524 shown in turquoise. All five models appear linear across the interval R_t on $[250, 275]$ K
 525 (right panel). It is possible that the shape of the response function $E(R)$ is neither linear nor
 526 exponential. However, the fact that, owing to the dominance of emission temperature in the
 527 climate system, R_1 is more than 92% of E_1 strongly suggests that large departures from
 528 linearity in equilibrium-temperature response are not to be expected.
 529

530 Even if Charney sensitivity were as little as 1.40 K in line with current midrange estimates of
 531 anthropogenic forcing and radiative imbalance assuming all industrial-era warming to be
 532 anthropogenic, as model 3 suggests, it is implausible that the feedback fraction in response to the pre-
 533 industrial NCGHGs would be as much as thrice that in response to emission temperature.

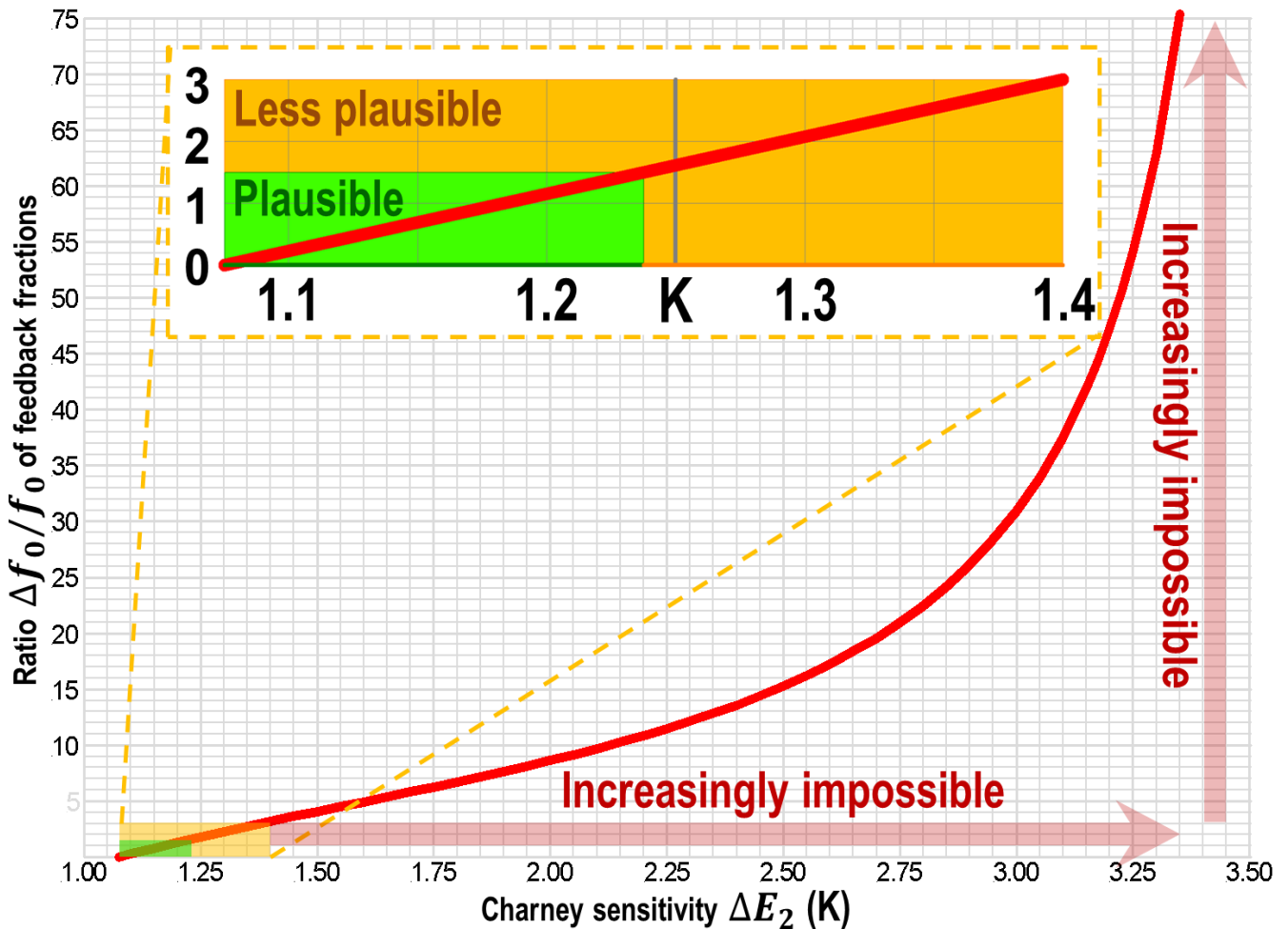
534 If Charney sensitivity is 1.15 K, as models 4, 5 suggest, the growth in the feedback response b in
 535 model 2 will be a plausible 0.5% per Kelvin of reference temperature, rather than the impossible
 536 $7\% \text{ K}^{-1}$ illustrated in model 2 (impossible because approximately logarithmic temperature response
 537 largely offsets exponential growth in specific humidity, giving a legitimate expectation of a near-linear
 538 response). The growth in the feedback fraction with temperature would likewise be plausible (Fig. 5).

539 The evolution of the feedback fraction f_t from emission temperature R_0 ($= 254.70 \text{ K}$) to reference
 540 temperature R_1 ($= 265.00 \text{ K}$) in 1850 (Fig. 6) reveals why it is that current projections of Charney
 541 sensitivity (model 1) are impossibly excessive. There is no physical basis for assuming that the ratio of
 542 the feedback fraction in response to the warming forced by the pre-industrial NCGHGs to the feedback
 543 fraction in response to emission temperature (the feedback-fraction ratio) will greatly exceed unity.



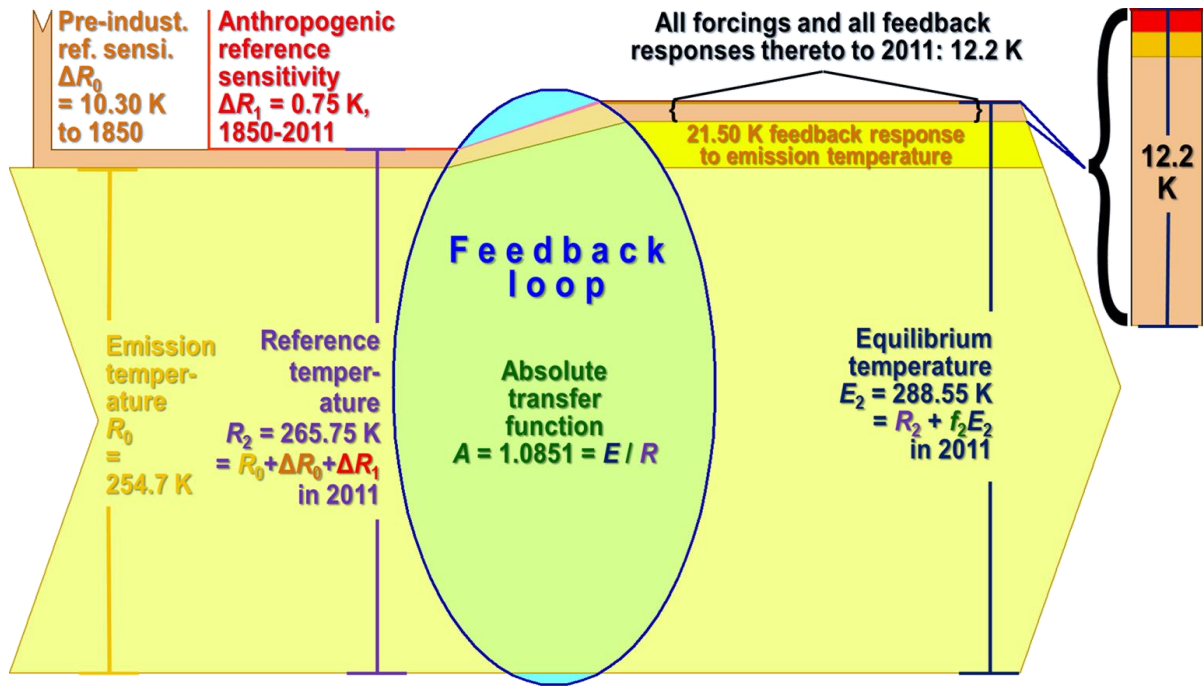
544
 545 **FIG. 6** Evolution of the feedback fraction f_t from emission temperature R_0 ($= 254.7 \text{ K}$) to
 546 reference temperature R_1 ($= 265.00 \text{ K}$) in 1850 and beyond.

547 Where $\Delta E_2 > 1.25 \text{ K}$, the ratio of Δf_0 ($= \Delta b_0/\Delta E_0$) to f_0 ($= b_0/E_0$) becomes unrealistically large.
 548 Thus, models 1 and 2 are impossible and model 3 is implausible, while models 4-5 are realistic. As Fig.
 549 7 shows, as the estimated Charney sensitivity rises above 1.4 K, the feedback-fraction ratio becomes so
 550 large as to imply a physically-unjustifiable growth in the feedback-fraction ratio. Since the sensitivity-
 551 altering temperature feedbacks in response to warming arising from increases in the atmospheric
 552 burden of the NCGHGs are precisely the same feedbacks that responded to the emission temperature
 553 consequent upon the fact that the Sun is shining, there is no reason to suppose that the feedback regime
 554 has changed or will change anything like as drastically as current equilibrium-sensitivity projections
 555 imply.



556
 557 **FIG. 7** The feedback-fraction ratio $\Delta f_0/f_0$, i.e., the ratio of the feedback fraction Δf_0 in
 558 in response to reference sensitivity to the pre-industrial NCGHGs and the feedback fraction f_0
 559 in response to emission temperature, for Charney sensitivity ΔE_2 on $[1.07, 3.35]$ K, for
 560 equilibrium temperature E_t an exponential-growth function $E(R)$ of reference temperature
 561 R_t . Green region: plausible sensitivities; orange region: implausible sensitivities. Beyond
 562 these, elevated feedback-fraction ratios and thus sensitivities are increasingly impossible.

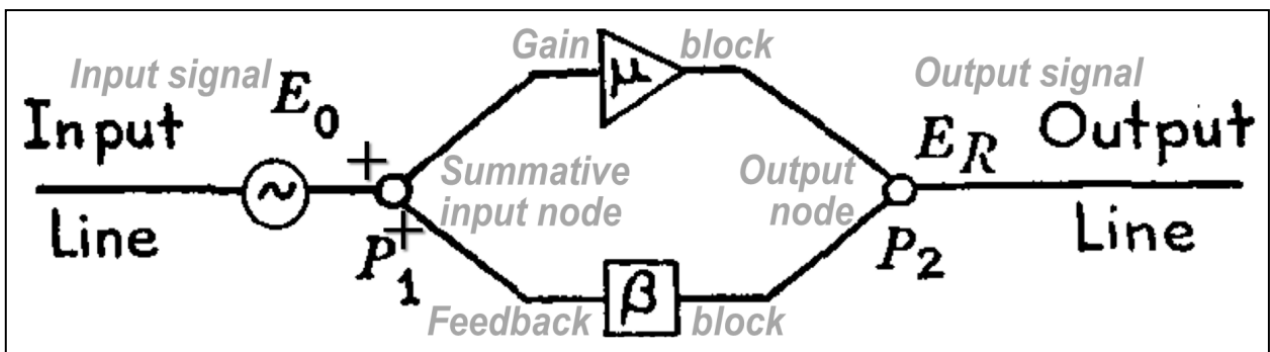
563 Block diagrams such as Fig. 3 do not show the relative magnitudes of the contributions to
 564 reference and equilibrium temperatures. Fig. 8, based on model 4, is an attempt to remedy this defect.
 565 Scaled temperature responses to anthropogenic forcings and feedback responses thereto are visibly
 566 small compared with the temperature responses to natural forcings and minuscule against emission
 567 temperature and the feedback response thereto. It is for this reason that, particularly under modern
 568 conditions, large variations in the feedback regime in response to the small anthropogenic perturbation
 569 of global temperature are not to be expected. The high equilibrium sensitivities that are currently
 570 projected effectively misallocate the large feedback response to emission temperature, improperly
 571 attributing it to anthropogenic increases in the NCGHGs.



572
 573 **FIG. 8** Relative magnitudes of the contributions to reference temperature R_2 and to
 574 equilibrium temperature E_2 in 2011, assuming $E_t = g(R_t) = R_t^x$ (model 4). Dominance of
 575 emission temperature (pale yellow) and its feedback response (bright yellow) is visible.

576 **7. Verification in the laboratory**

577 In climate, individual temperature feedbacks cannot be measured. However, feedback theory (Bode,
 578 1945: Fig. 9) applies no less to climate than to the electronic networks for which it was derived. Since
 579 states of a circuit can be directly measured more reliably than states of the climate, testing at two
 580 laboratories using circuits designed to represent features of the climate verified the theory outlined here.



581
 582 **FIG. 9** A feedback amplifier with a μ gain block and a β feedback block (Bode 1945)

583 Based on a circuit built at the laboratory of an author (Whitfield) to simulate feedback loops
 584 electronically, a government laboratory built and ran a more sensitive rig. The input signal (E_0 in Bode
 585 1945, p. vii), the open-loop gain factor μ and the feedback ratio β in Fig. 9 could be varied, whereupon
 586 the output signal (Bode's E_R) could be measured directly. The laboratory was given 23 sets of three
 587 values in four test groups and configured the circuit using each set, measuring the output signal in a
 588 temperature-controlled chamber.

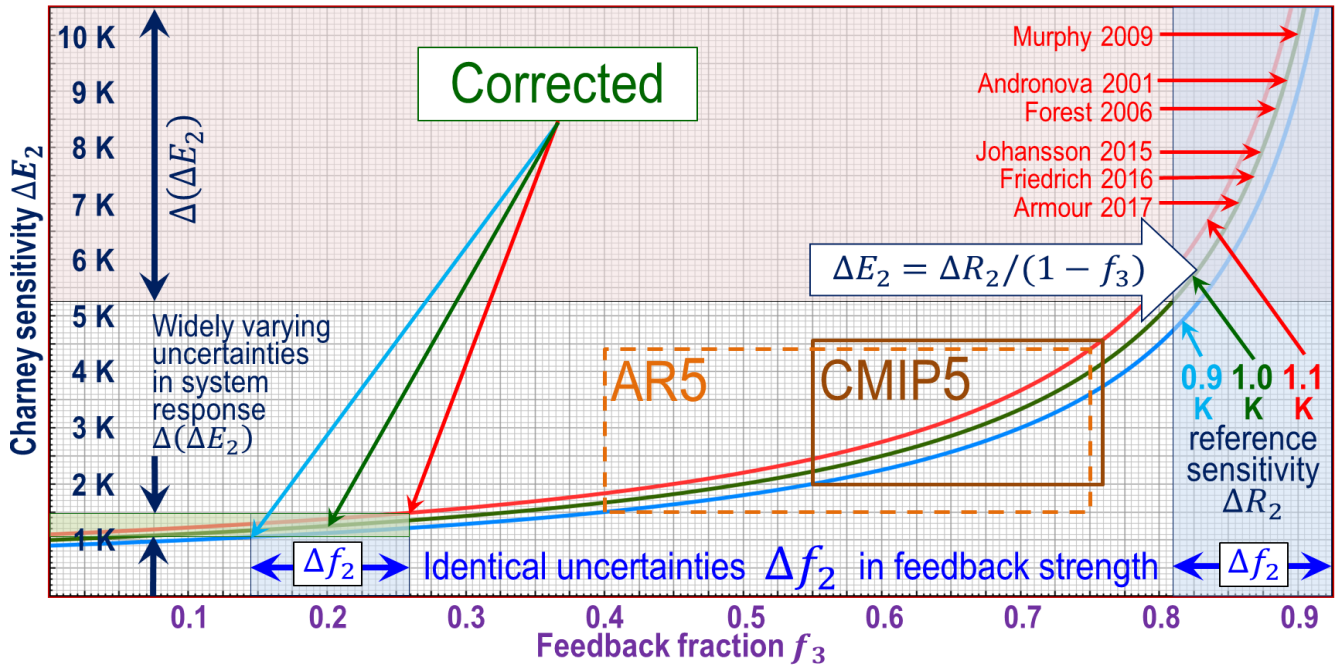
589 After some months' delay owing to heat from the presence of the operator, which entailed revision
 590 of the inputs to yield the required precision without invalidating the tests, the laboratory reported.
 591 Results of all 23 tests, given in supplementary matter at S1 and reported by the laboratory at S2, agreed
 592 with the theory discussed here to a precision equivalent to 0.1 K. To overcome variances in the
 593 performance of individual components in the test circuit, each input value was measured to ensure that
 594 it was within tolerance. The result from test group 3 showed that, even without any amplification, i.e.,
 595 where $\mu := 1$ in Fig. 9, any output signal E drives a feedback response where feedbacks are present.
 596 Results for all test groups were as follows:

- 597 1. For $f_3 (= \mu\beta)$ on $(f_{\text{mid}})_3 \pm 40\%$ (from Vial et al., 2013) and $\Delta R_2 = 1.16$ K (based on Myhre et
 598 al. 1998 and IPCC 2001), and even before correcting the error identified here, Charney
 599 sensitivity ΔE_2 falls on 2.3 [1.6, 3.6] K and not on the CMIP5 interval 3.35 [2.1, 4.7] K.
- 600 2. Where absolute input and output signals R_3, E_3 replace $\Delta R_2, \Delta E_2$ the interval of Charney
 601 sensitivities ΔE_2 narrows from 3 K to < 1 K, and the upper bound falls. From this experiment,
 602 current overstatements of the feedback factor f_t and the system-gain function A_t were first
 603 noticed.
- 604 3. Even where $\mu := 1$ (i.e., the input signal is unamplified), the output signal exceeds it by the
 605 expected margin in the presence of positive feedback; and, where $\mu > 1$, the output signal does
 606 not much exceed the value for $\mu := 1$. This experiment revealed the magnitude of the error of
 607 neglecting the feedback response to absolute temperatures.
- 608 4. After correction of climatology's error of definition, the magnitude and interval breadth of
 609 output responses to absolute system-gain functions A_t are small.

610 8. Uncertainties

611 The fact that feedback responds not only to anthropogenic reference sensitivity but also to reference
 612 sensitivity to the pre-industrial NCGHGs and also, most importantly, to emission temperature powerfully
 613 constrains the uncertainty as to the shape of the equilibrium-temperature response function $E(R)$. It has
 614 been demonstrated here that the steep exponential-growth scenarios implicit in current estimates of
 615 Charney sensitivity are impossible because they imply a feedback response to NCGHGs that exceeds by
 616 orders of magnitude the feedback response to emission temperature.

617 Thus, uncertainty in Charney sensitivity ΔE_2 is small, because even large uncertainties in absolute
 618 temperatures entail small uncertainties in their ratio, the absolute system-gain factor A . Furthermore,
 619 the Charney-sensitivity interval obtained via A (Eq. 1) falls on the near-linear region near the origin of
 620 the hyperbolic curve of Charney-sensitivity response to feedback fractions f_3 (Fig. 10).



621
622 **FIG. 10** The rectangular-hyperbolic response curves of Charney sensitivities ΔE_2 against
623 feedback factors f_3 for reference sensitivity ΔR_2 on $1.0 \text{ K} \pm 10\%$. Identical uncertainties Δf_2
624 in f_3 generate broader uncertainty intervals $\Delta(\Delta E_2)$ in system response ΔE_2 as $f_3 \rightarrow 1$,
625 since $\Delta(\Delta E_2)$ depends greatly on f_3 (Roe 2009, fig. 6). High-end predictions of ΔE_2 from
626 six sources, the CMIP5 GCMs' interval [2.1, 4.7] K and the 2σ interval 1.15 [1.10, 1.25] K
627 from Eq. (1) are shown. Varying f_3 visibly makes very much more difference to ΔE_2 than
628 varying ΔR_2 , particularly where $f_3 \rightarrow 1$.

629 Since there is little uncertainty in deriving $A_3 = 1.085$, Charney sensitivity $\Delta E_2 = 1.15 \text{ K}$. Though
630 there are uncertainties in deriving $\Delta E_1, \Delta R_1$ for 2011, the values of both sensitivities are so small when
631 set against E_1, R_1 (R_1 being > 350 times ΔR_1) that they barely perturb A .

632 Allowance should also be made for Hölder's inequalities between integrals in deriving emission
633 temperature R_0 . Integrating latitudinal temperatures on the dayside of an ice planet, the hemispheric
634 mean temperature would be 240.6 K assuming today's insolation with uniform albedo 0.66. However,
635 this value becomes 268.5 K assuming mean ocean surface albedo 0.06 in the ice-free tropics, since, to
636 first-order approximation, at today's insolation one-third of the dayside surface area would be ice-free
637 even before taking account of evapotranspiration and temperature feedbacks. Allowing for a nightside
638 temperature of $\sim 240 \text{ K}$ (based on Merlis 2010), global mean emission temperature in the absence of
639 greenhouse gases or of temperature feedbacks would be $\sim 255 \text{ K}$, coincidentally near-identical with the
640 value derived using a single global application of the Stefan-Boltzmann equation at today's albedo 0.3.

641 Industrial-era uncertainties, though greater than in 1850, barely affect $A_2 = 1.085$ in Eq. (1). An
642 empirical campaign (Table 9), drawing upon ten authoritative sources for anthropogenic radiative
643 forcing over various periods in the industrial era, established that in each of the ten cases A_2 fell on the
644 interval [1.085, 1.088]. However, as cols. 7, 8 of Table 9 indicate, in the current method uncertainty is
645 considerable: the upper bound of the partial system-gain factor a_2 is not 1.08 but 3.74. To the nearest
646 0.05 K, all ten data sources generate Charney sensitivity $\Delta E_2 = 1.15 \text{ K}$ (Col. 10).

TABLE 9 System-gain factors A_2 and Charney sensitivities ΔE_2 in the industrial era to 2011

		ΔQ_1	ΔN_1	ΔT_1	ΔR_1	ΔE_1	ΔE_1	a_2	A_2	ΔE_2	ΔE_2
		$-\text{W m}^{-2}$	$-\text{K}$	K	K	K	K	Unitless	Unitless	K	K
Data source	Year	1	2	3	4	5	6	7	8	9	10
Miller 2014	2012	2.95	0.60	0.76	0.91	2.88	0.95	1.04	1.085	1.11	1.15
Myhre 2017	2016	3.10	0.60	0.84	0.96	3.03	1.04	1.08	1.085	1.16	1.15
IPCC AR5 2013	1980	1.25	0.40	0.38	0.39	1.22	0.56	1.44	1.086	1.54	1.15
Knutti 2002	2001	1.90	0.50	0.62	0.59	1.86	0.84	1.43	1.086	1.53	1.15
IPCC AR5 2013	1950	0.57	0.20	0.26	0.18	0.56	0.40	2.27	1.086	2.42	1.15
IPCC AR5 2013	2011	2.29	0.60	0.76	0.71	2.24	1.03	1.45	1.086	1.55	1.15
Haywood 2007	2006	1.93	0.50	0.68	0.60	1.88	0.92	1.53	1.086	1.64	1.15
IPCC AR4 2007	2005	1.60	0.50	0.67	0.50	1.56	0.97	1.96	1.087	2.10	1.15
Skeie 2011	2010	1.40	0.60	0.74	0.43	1.37	1.30	2.98	1.088	3.19	1.15
Boucher 2001	2000	1.00	0.50	0.58	0.31	0.98	1.16	3.74	1.088	4.00	1.15

648

Col. 1: Net anthropogenic forcing ΔQ_1 to year shown, given by the listed source authority;

649

Col. 2: Estimated radiative imbalance ΔN_1 (based on Smith et al., 2015);

650

Col. 3: Observed warming ΔT_1 from 1850 to the end year shown (Morice et al., 2012);

651

Col. 4: Period reference sensitivity $\Delta R_1 = \Delta Q_1 P_2$;

652

Col. 5: Current period equilibrium sensitivity $\Delta E_1 = \Delta R_1 (A_M)_2 \quad | \quad (A_M)_2 = 3.14$;

653

Col. 6: Revised period equilibrium sensitivity $\Delta E_1 (= \Delta T_1 \Delta Q_1 / (\Delta Q_1 - \Delta N_1))$;

654

Col. 7: Current system-gain factor $a_2 \approx \Delta E_1 / \Delta R_1$ (i.e., Col. 5 / Col. 4);

655

Col. 8: Revised system-gain function $A_2 \approx E_2 / R_2$;

656

Col. 9: Current Charney sensitivity $\Delta E_2 = \Delta Q_2 P_2 a_2$ (i.e., $\Delta Q_2 P_2 \times$ Col. 7); and

657

Col. 10: Revised Charney sensitivity $\Delta E_2 = \Delta Q_2 P_2 A_2$ (i.e., $\Delta Q_2 P_2 \times$ Col. 8), to nearest 0.05 K.

658

The 2σ uncertainties in Charney sensitivity ΔE_2 were computed via a Monte Carlo process. First,

659

the uncertainty in each variable on which ΔE_2 depends was specified. Normal distributions were used,

660

with the parameters derived from each variable's midrange estimate and stated 2σ uncertainty bounds,

661

under the conservative assumption that the uncertainties in all such variables were mutually

662

independent. Charney sensitivity ΔE_2 depends on ΔR_2 (which in turn depends on $\Delta Q_2, P_2$), and on f_1

663

(which in turn depends on $R_0, \Delta R_0$). Thus, ΔQ_2 was taken as $3.447 \text{ W m}^{-2} \pm 5\%$; P_2 as

664

$0.305 [0.295, 0.315] \text{ K W}^{-1} \text{ m}^2$; R_0 as $254.7 \text{ K} \pm 5\%$; ΔR_0 was $10.3 [8.9, 11.7] \text{ K}$; and E_1 as

665

$287.55 \pm 0.05 \text{ K}$ in 1850 (Morice et al., 2012).

666

The overall uncertainty in ΔE_2 was obtained by simulating $n = 300,000$ draws from each variable

667

on which ΔE_2 depends. Additional draws for the feedback fraction f_1 were made and inserted into Eq.

668

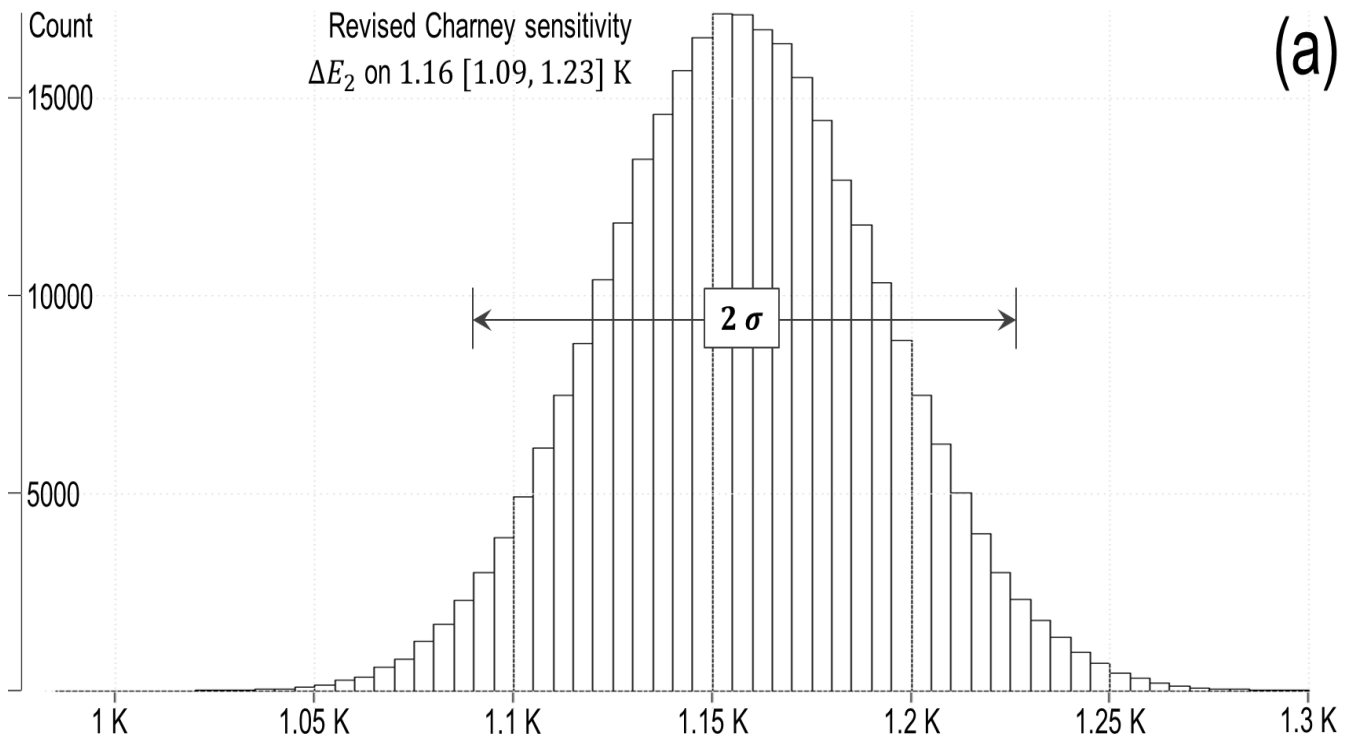
(1) to obtain ΔE_2 . For comparison, the uncertainty in ΔE_2 was likewise obtained using the CMIP5

669

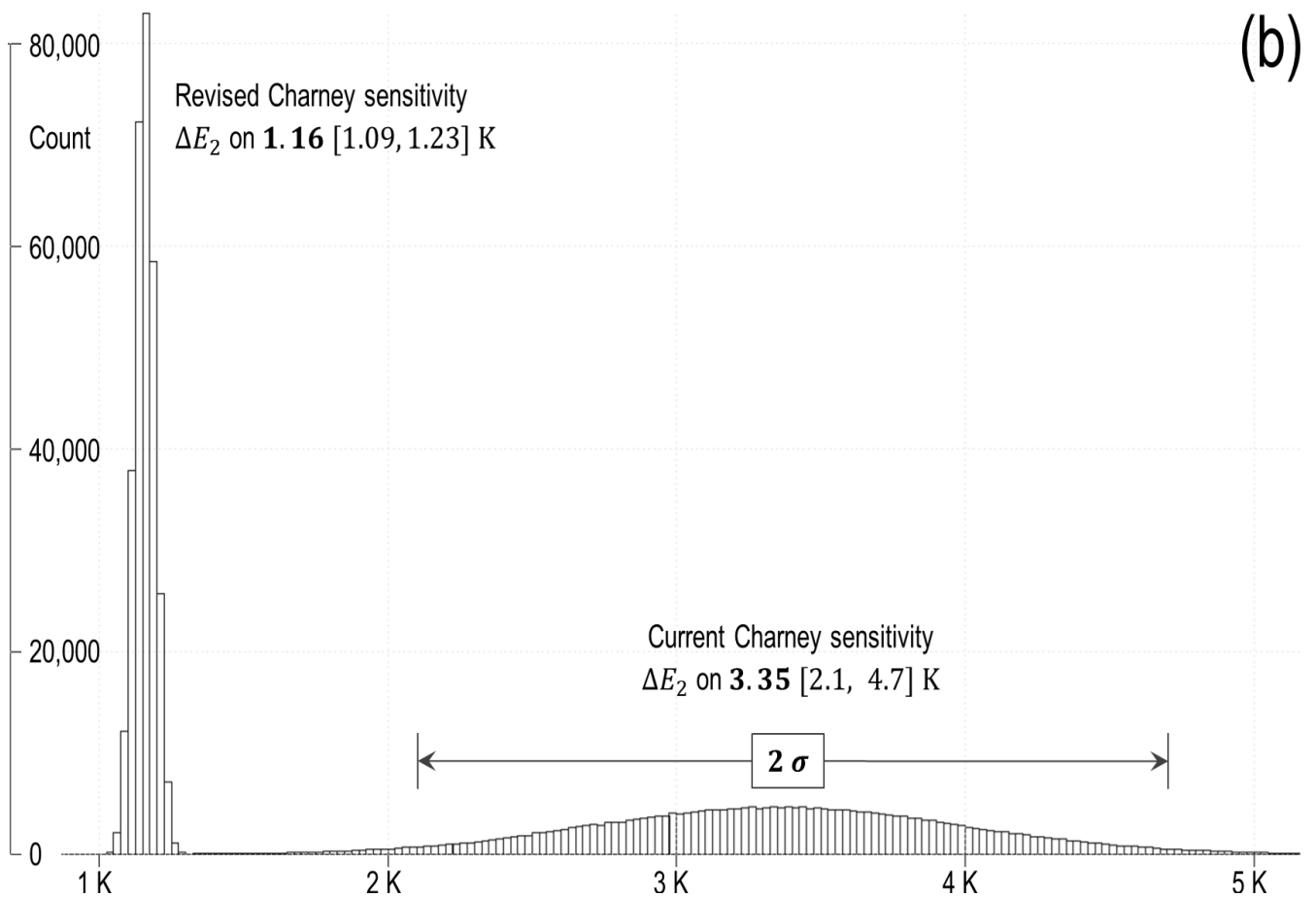
ensemble's implicit feedback fraction $(f_M)_2$. The 2σ bounds were estimated directly from the samples

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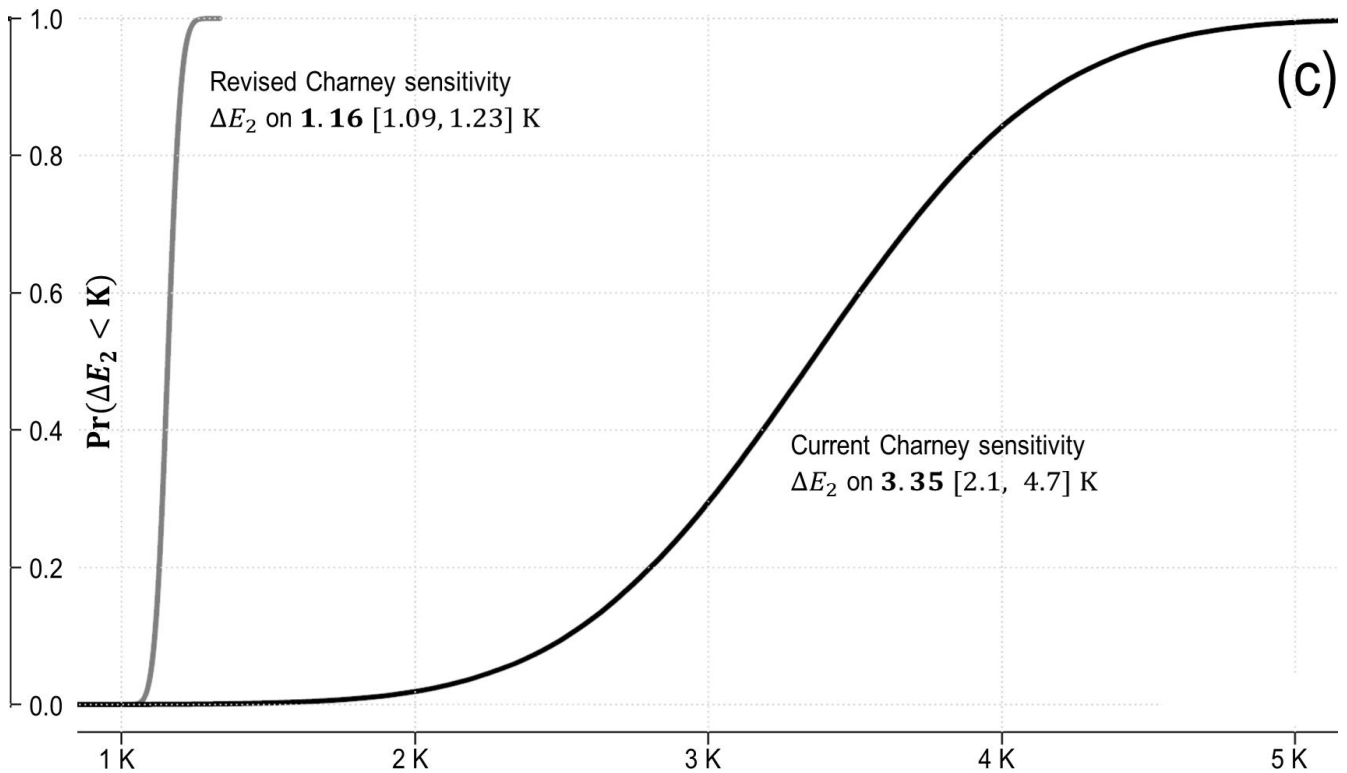
(Fig. 11).



671
 672 **FIG. 11 (a)** Monte Carlo distribution of Charney sensitivities ΔE_2 revised after correction
 673 of the error in defining temperature feedback identified herein. Bin widths are 0.005 K.



674
 675 **FIG. 11 (b)** Scaled comparison of Monte Carlo distributions for revised (left) against
 676 current (right) Charney sensitivities ΔE_2 . Here, bin widths are 0.025 K.



678

679 **FIG. 11 (c)** Cumulative distributions of probability that Charney sensitivity is less than a
 680 given value in K for revised (gray) against current (black) Charney sensitivities ΔE_2 .

681

682 There is no consensus on the anthropogenic fraction of warming since 1850 (Legates et al., 2015).
 Here it is assumed to be 100%. If it is $< 100\%$, equilibrium sensitivity ΔE_2 may be less than shown.

683

9. Discussion and conclusion

684

685 Climatology erroneously defines temperature feedback as responding solely to anthropogenic
 686 perturbation, when feedback also responds to emission temperature and to natural perturbations thereof.

687

688 This error of definition has engendered many consequential errors. For instance, climatology defines
 689 the partial system-gain factor a as the secant-slope of the curve of the equilibrium-sensitivity function

690

691 $E(R)$, when it is demonstrated here that, regardless of the shape of $E(R)$, the true system-gain factor A_t
 692 at any time t is simply the ratio of E_t to R_t . Furthermore, climatology implicitly assumes not only that
 693 equilibrium sensitivity is time-independent but also that feedback response (especially the response to
 694 the water-vapor feedback) is exponential, when in truth feedback response, even to the water-vapor
 695 feedback, is close to linear, so that equilibrium sensitivity is at worst weakly time-dependent.

696

697 Though the shape of the equilibrium-temperature response function $E(R)$ is unknown, in models
 698 1-4 it is here assumed to be an exponential-growth curve. The reason is that any net-growth curve other
 699 than an exponential-growth curve will, at some point t , demonstrate a still larger and still less plausible
 700 difference between the feedback fraction in response to emission temperature and the feedback fraction
 701 in response to a subsequent natural or anthropogenic perturbation of emission temperature.

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698 Not the least reason why near-linearity in today’s temperature-feedback regime is to be expected is
699 that reference sensitivity R_1 in 1850 is 92% of equilibrium sensitivity E_1 . Consequently, climatology’s
700 method implies that the feedback response to the NCGHGs exceeds the feedback response to emission
701 temperature by one or even two orders of magnitude. Any such elevated feedback-fraction ratio is
702 impossible, particularly given that the reference-sensitivity interval of interest, $[R_0, R_3]$, is narrow.

703 Correction of these errors by the use of the absolute system-gain factor A_t in Eq. (1) gives rise to a
704 well constrained expectation of 1.15 [1.10, 1.25] K Charney sensitivity. That interval is in line with
705 observation (Fig. 1) and with current estimates of net anthropogenic forcing in the industrial era. By
706 contrast, the more volatile equation (Eq. 2) currently universally adopted in climatology delivers an
707 interval excessive both in its magnitude and in its long-unconstrained breadth.

708 Once the large feedback response to the entire reference signal R_2 rather than solely to the
709 anthropogenic perturbation ΔR_1 is correctly accounted for, the absolute system-gain factor A_3 and thus
710 Charney sensitivity ΔE_2 prove to be well below current estimates. Since the CMIP3/5 ensemble
711 implicitly assumes a system-gain factor $(A_M)_3 = 3.2$ (based on data in Andrews et al. 2012), deploying
712 that assumption in Eq. (2) suggests models over-predict global warming to a greater extent than
713 authorities such as Millar et al. (2017) have suggested. The revised midrange Charney sensitivity, at
714 1.15 K, is one-third of the implicit 3.35 K midrange CMIP5 estimate (also derived from Andrews, *op.*
715 *cit.*). Contrary to suggestions (e.g. by Frame & Stone, 2013) that predictions in IPCC (1990) were
716 accurate, the data underlying both Fig. 1 and the empirical campaign (Table 9) suggest that current
717 GCMs very greatly overstate the system-gain factor and consequently Charney sensitivity.

718 Many explanations for the discrepancy between prediction and observation (Fig. 1) exist. Grose et
719 al. (2017) suggest “global warming holes” (regions warming more slowly than average). Rahmstorf et
720 al. (2012) find that removing short-term cooling influences like La Niña aligns the predictions in IPCC
721 (1990) with observation. Occam’s Razor, however, suggests that the substantial credibility gap between
722 predicted and observed warming rates persists because GCMs’ outputs reflect the definitional error
723 identified here. Consequently, substantial overestimates of global warming have been made throughout
724 the 120 years since Arrhenius (1896, table VII) first estimated Charney sensitivity as ~ 5.5 K.

725 Though IPCC has hitherto assigned ever-greater “certainties” to the notion that recent warming was
726 chiefly anthropogenic, that notion – poorly supported in the journals (Legates et al. 2015) – arises from
727 the error of physics described here. Insofar as GCMs’ equilibrium sensitivities reflect results obtained
728 exclusively via Eq. (2), those sensitivities are greatly overstated. Climatology’s attempt to apply a
729 concept from experimental science in an observational-science setting has not succeeded. It is now
730 advisable greatly to reduce what Hourdin et al. (2017) call the “anticipated acceptable range” of
731 equilibrium sensitivities that models have hitherto been tuned to deliver. These results imply that, even
732 without mitigation, there will be little net harm from the slow, small global warming that is to come.

DISCLOSURE STATEMENT

734

735 No author has received any grant or other emolument for this work. None has a proprietary interest in
736 any relevant undertaking. Christopher Monckton of Brenchley received fees and travel expenses from
737 the Science and Public Policy Institute from 2007-2009; he also received travel expenses for attending
738 conferences from the Committee for a Constructive Tomorrow from 2006-2013, from the Heartland
739 Institute from 2007-2017, from the World Federation of Scientists in 2010; from the Moscow City
740 Government in 2018, from Camp Constitution in 2018-2019, and from the Deutscher Bundestag in
741 2019. Dr Willie Soon, as a solar astrophysicist at the Harvard-Smithsonian Center for Astrophysics
742 (here speaking only for himself), is paid out of grants (some from fossil-fuel interests) negotiated by the
743 Center for him, but has received nothing for this work; Dr David Legates, as Professor of Climatology
744 in the University of Delaware, Dr William M. Briggs, as emeritus professor of statistics in the Weill
745 School of Medicine at Cornell University, and Dr Dietrich Jeschke, as professor of energy and
746 biotechnology in the Flensburg University of Applied Sciences, Germany, have received salaries or
747 grants for research in climatology, in probability and statistics and in control theory respectively, but
748 not in respect of the present work; Dipl.-Ing. Michael Limburg is vice-president of the Europäisches
749 Institute für Klima und Energie; Alex Henney has in the past received fees for advice on electricity
750 markets in the U.S. and elsewhere; John Whitfield is a retired electronics engineer; and James
751 Morrison, as an environmental consultant, has in the past received fees for marketing wind turbines.
752 Some authors act as unpaid advisors to the Heartland Institute.

753

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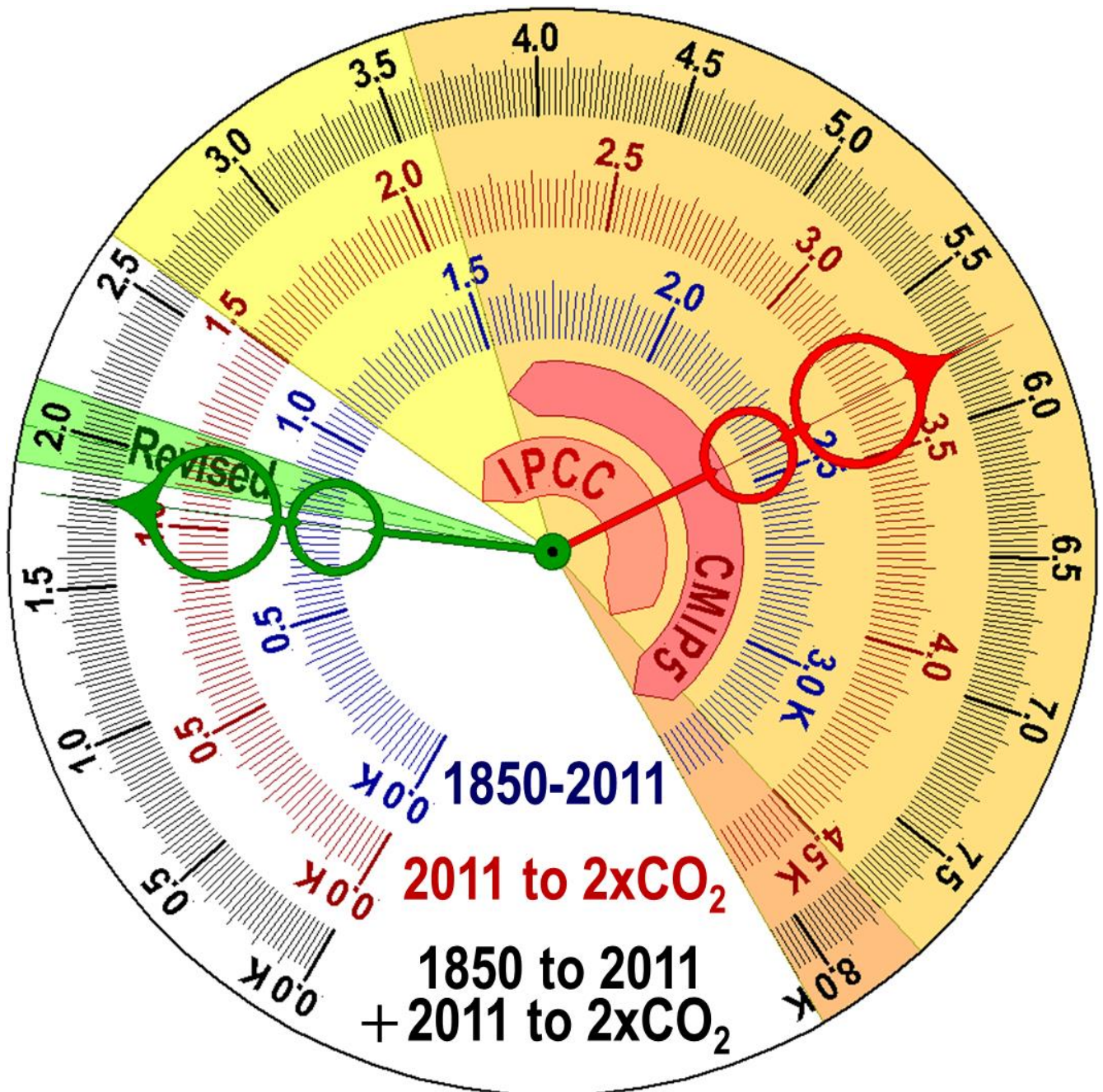
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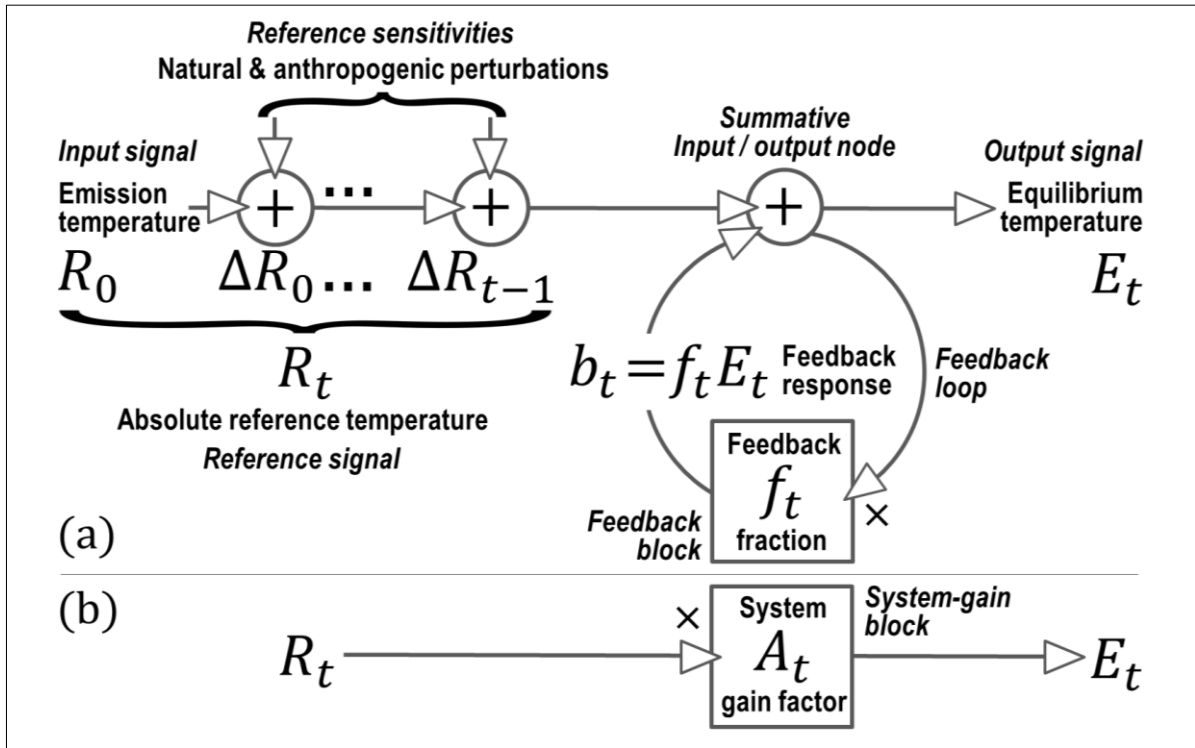
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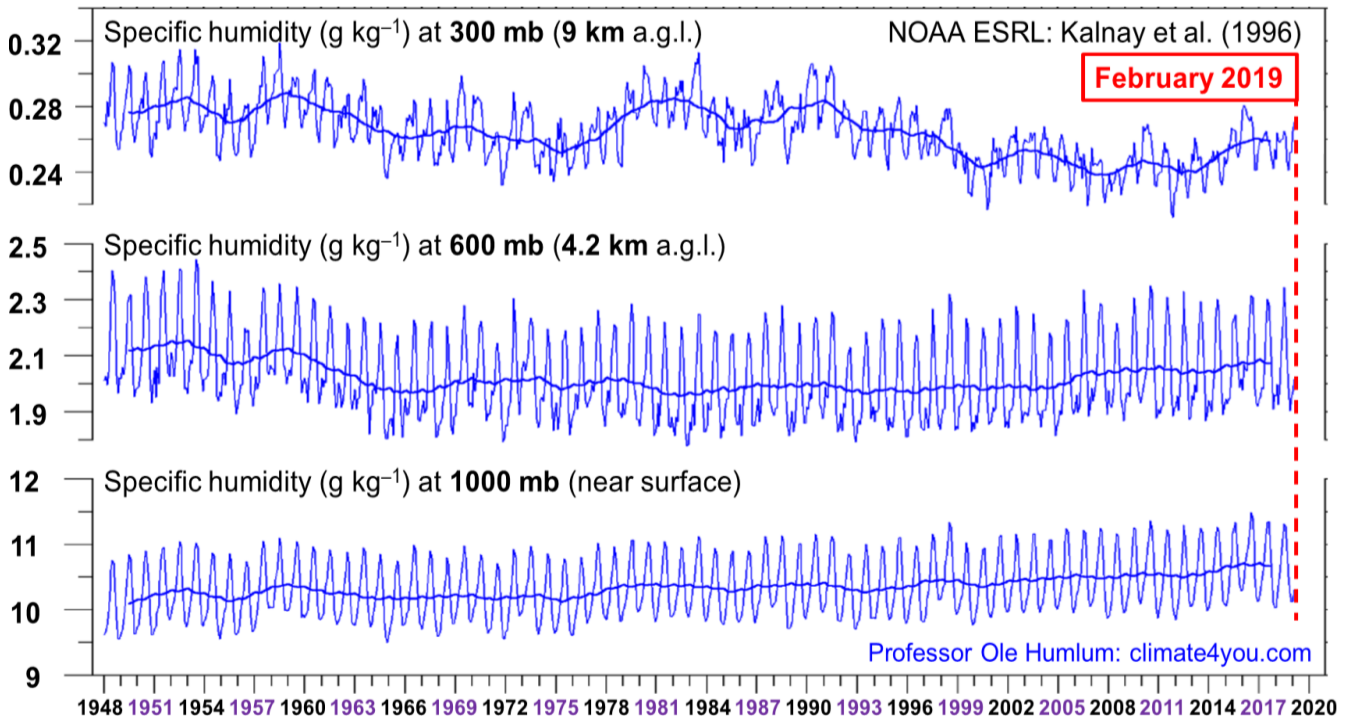
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FIG. 1. Overlapping projections by IPCC (2013) and CMIP5 (Andrews et al. 2012) of global warming from 1850-2011 (**blue scale**), in response to doubled CO₂ (**red scale**) and the sum of these two (**black scale**) greatly exceed warming equivalent to the 0.75 K observed from 1850-2011 (HadCRUT4: **green needle**). The 3.35 K CMIP5 mid-range Charney sensitivity (**red needle**) implies 2.4 K anthropogenic warming by 2011, about thrice observation. The revised warming interval derived herein (**pale green region**) is consistent with observed warming to 2011 (**green needle**).



951
 952 **FIG. 2.** The *feedback loop* (a) simplifies to (b), the schematic for the **system-gain factor** A_t
 953 at time t . The *reference signal* (reference temperature R_t), the sum of the *input signal*
 954 (emission temperature R_0), and all *perturbations* (reference sensitivities $\Delta R_0, \dots, \Delta R_{t-1}$), is
 955 input via the *summative input/output node* to the feedback loop. The *output signal*
 956 (equilibrium temperature E_t), is the sum of R_t and the **feedback response** $b_t := f_t E_t$ ($:=$
 957 $E_t - R_t$). Then $A_t (= E_t/R_t)$ is equal to the sum $\sum_{i=0}^{\infty} f_t^i = (1 - f_t)^{-1}$ of the infinite
 958 convergent geometric series $\{f_t^0 + f_t^1 + \dots + f_t^{\infty}\}$ under the convergence criterion $|f_t| <$
 959 1. The *feedback block* (a) and the *system-gain block* (b) must perforce act not only on the
 960 anthropogenic perturbation ΔR_{t-1} but on the entire reference signal R_t .

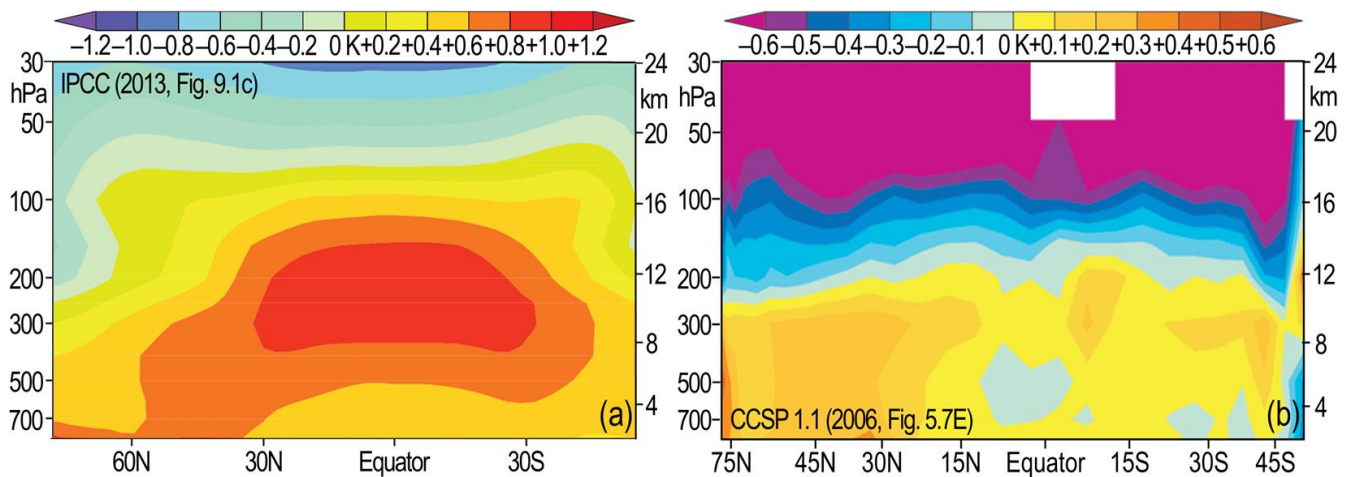


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FIG. 3 Specific humidity (g kg^{-1}) at 300, 600 and 1000 mb

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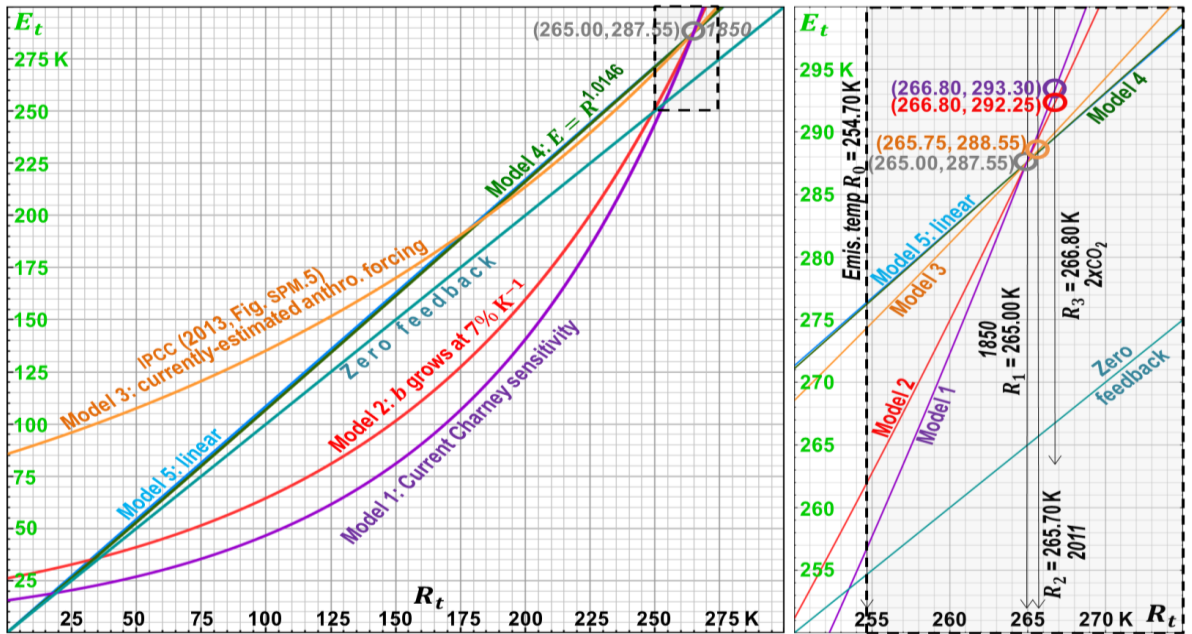
965

FIG. 4. | GCMs' projected "hot spot"²⁸ (a) is absent in observational data¹¹ (b).

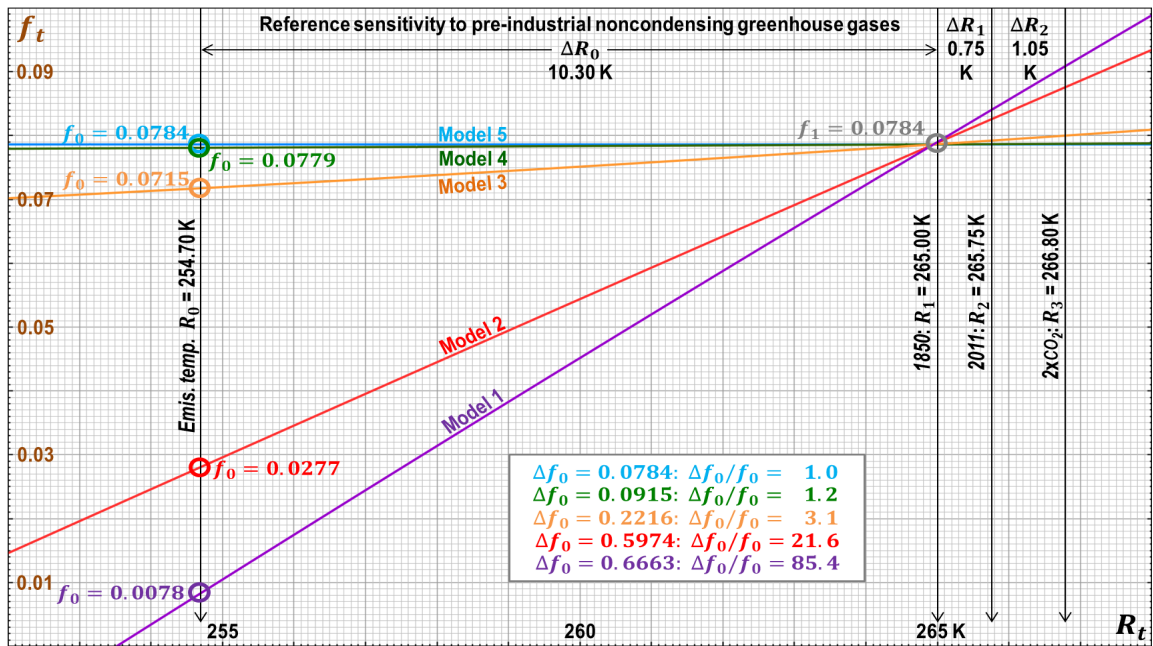
966

Temperature anomalies (in Kelvin) are color-coded.

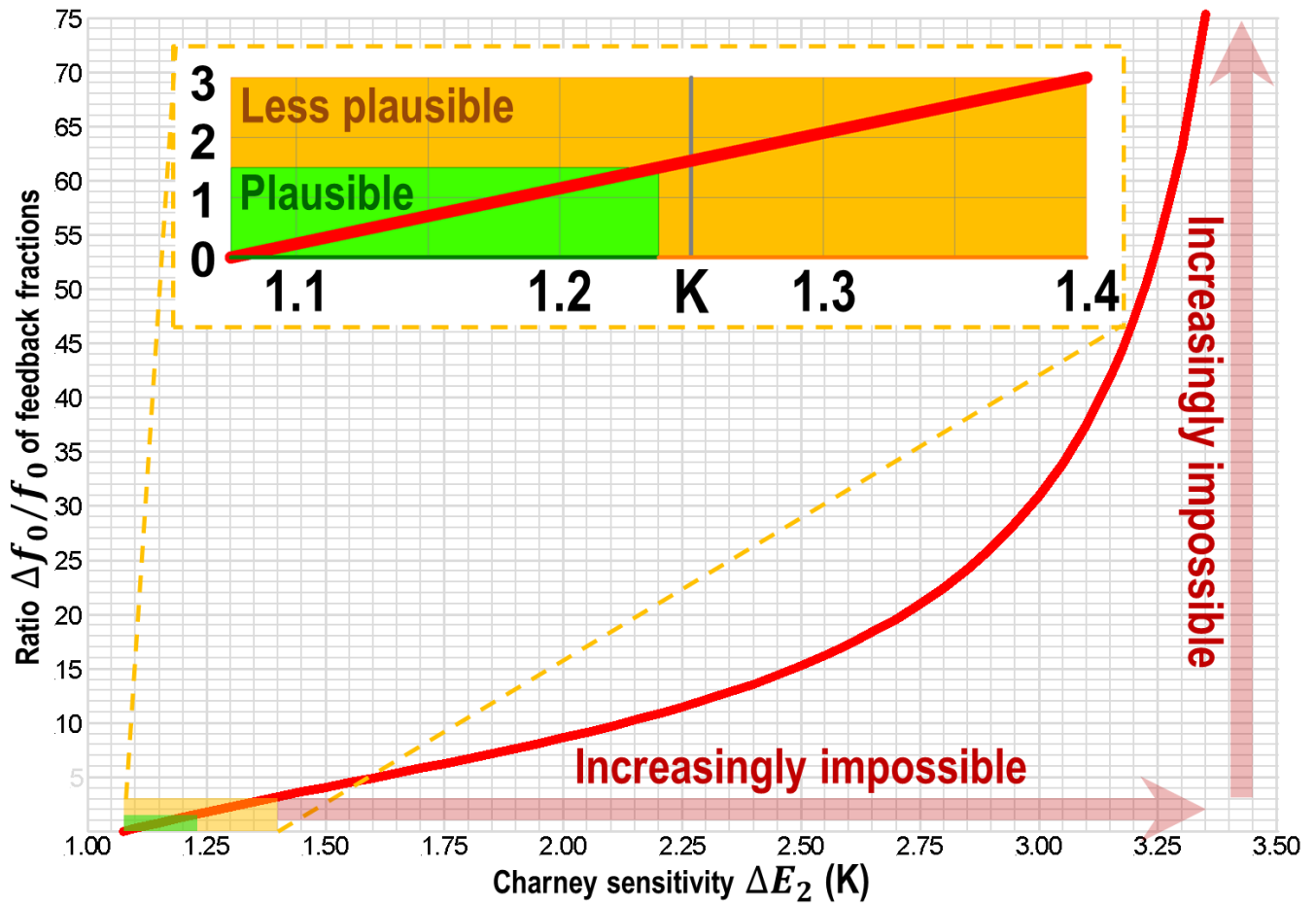
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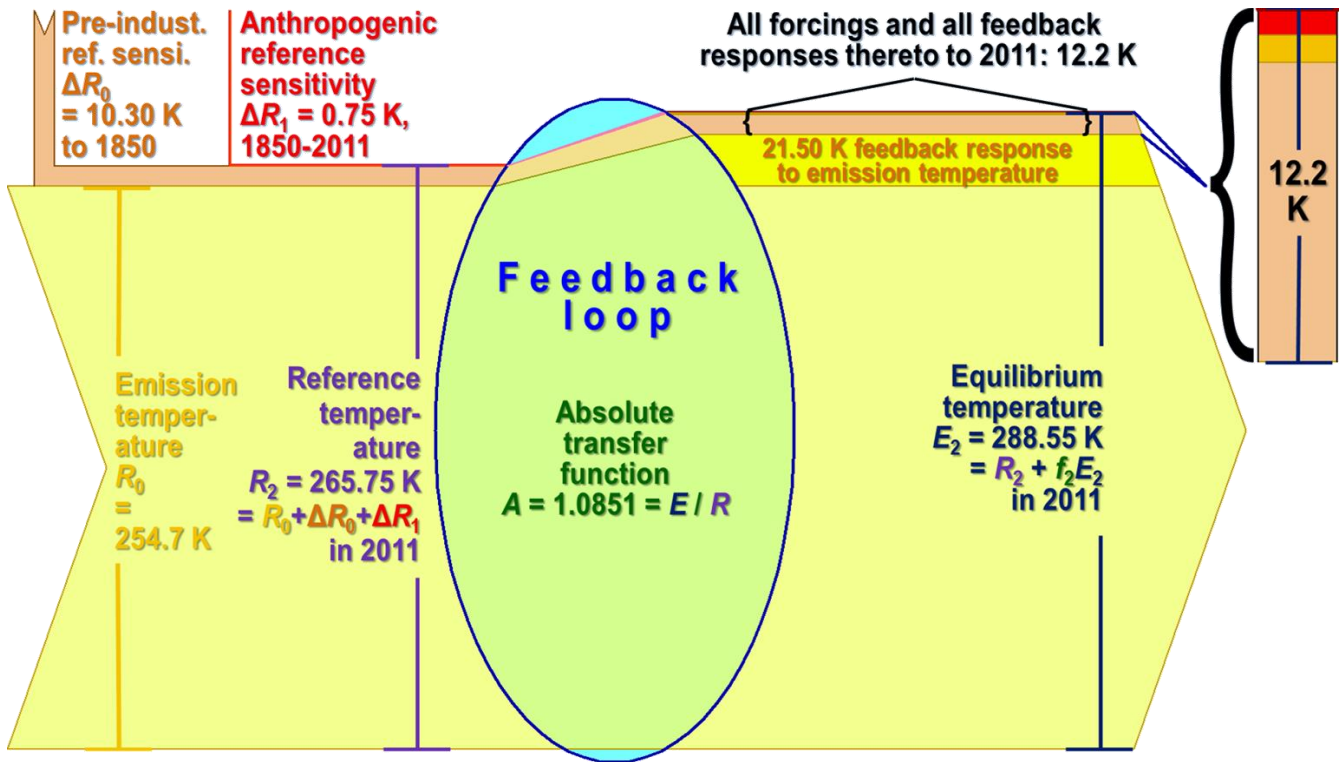
968
 969 **FIG. 5** Comparison of the five models of the evolution of $E(R)$ for R on $[250, 275]$ K.
 970 Models 1 (purple), 2 (red) and 3 (orange) are each generated from two points: the circled
 971 points in their colors and the common gray point $(265.00, 287.55)$ representing the
 972 position in 1850. In model 4 (green), the exponent $x = \ln(287.55)/\ln(265.70) = 1.0146$.
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 974 shown in turquoise. All five models appear linear across the interval R_t on $[250, 275]$ K
 975 (right panel). It is possible that the shape of the response function $E(R)$ is neither linear nor
 976 exponential. However, the fact that, owing to the dominance of emission temperature in the
 977 climate system, R_1 is more than 92% of E_1 strongly suggests that large departures from
 978 linearity in equilibrium-temperature response are not to be expected.



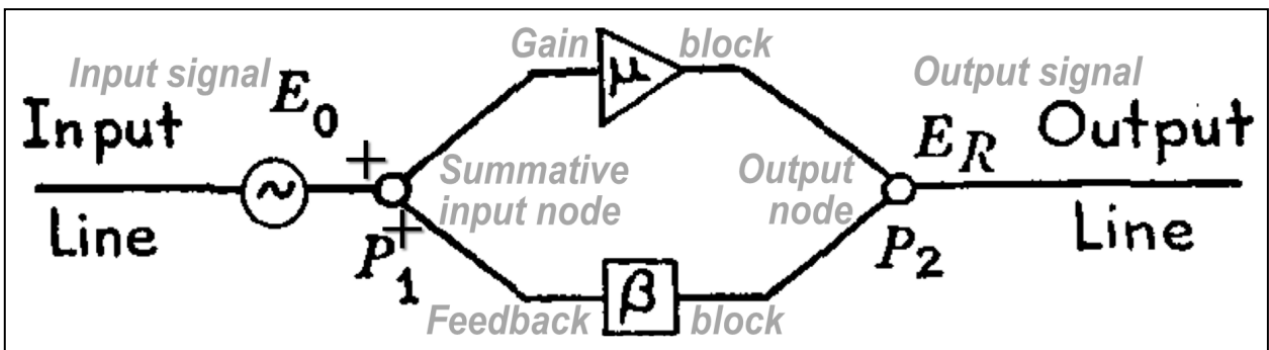
979
 980 **FIG. 6** Evolution of the feedback fraction f_t from emission temperature R_0 ($= 254.7$ K) to
 981 reference temperature R_1 ($= 265.00$ K) in 1850 and beyond.



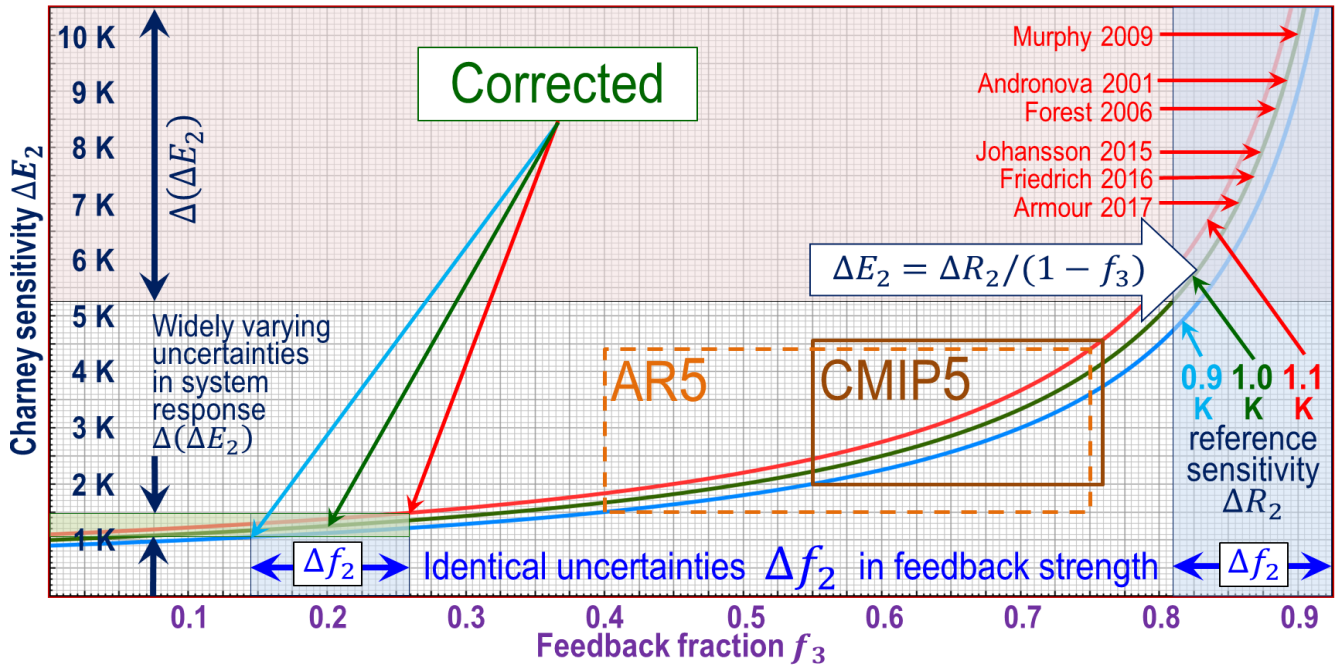
982
 983 **FIG. 7** The feedback-fraction ratio $\Delta f_0/f_0$, i.e., the ratio of the feedback fraction Δf_0 in
 984 in response to reference sensitivity to the pre-industrial NCGHGs and the feedback fraction f_0
 985 in response to emission temperature, for Charney sensitivity ΔE_2 on $[1.07, 3.35]$ K, for
 986 equilibrium temperature E_t an exponential-growth function $E(R)$ of reference temperature
 987 R_t . Green region: plausible sensitivities; orange region: implausible sensitivities. Beyond
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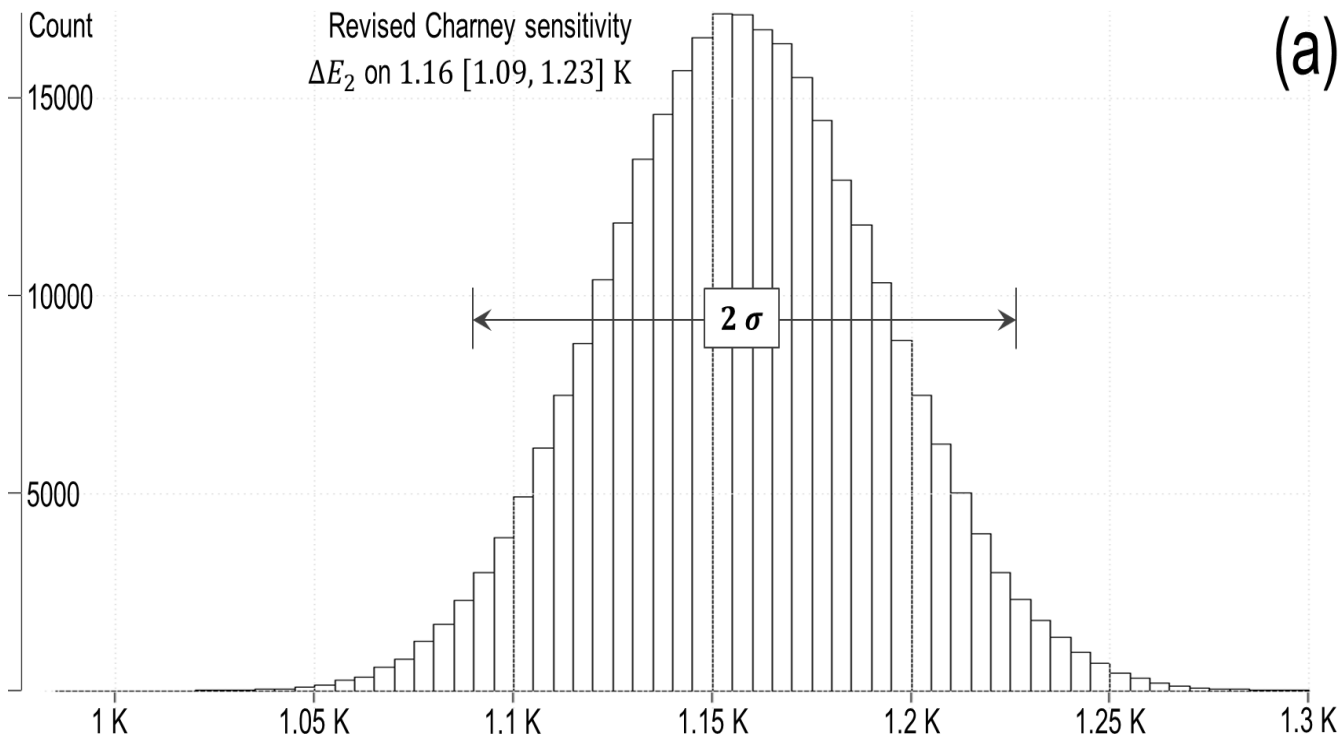
990
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 992 equilibrium temperature E_2 in 2011, assuming $E_t = g(R_t) = R_t^x$ (model 4). Dominance of
 993 emission temperature (pale yellow) and its feedback response (bright yellow) is visible.



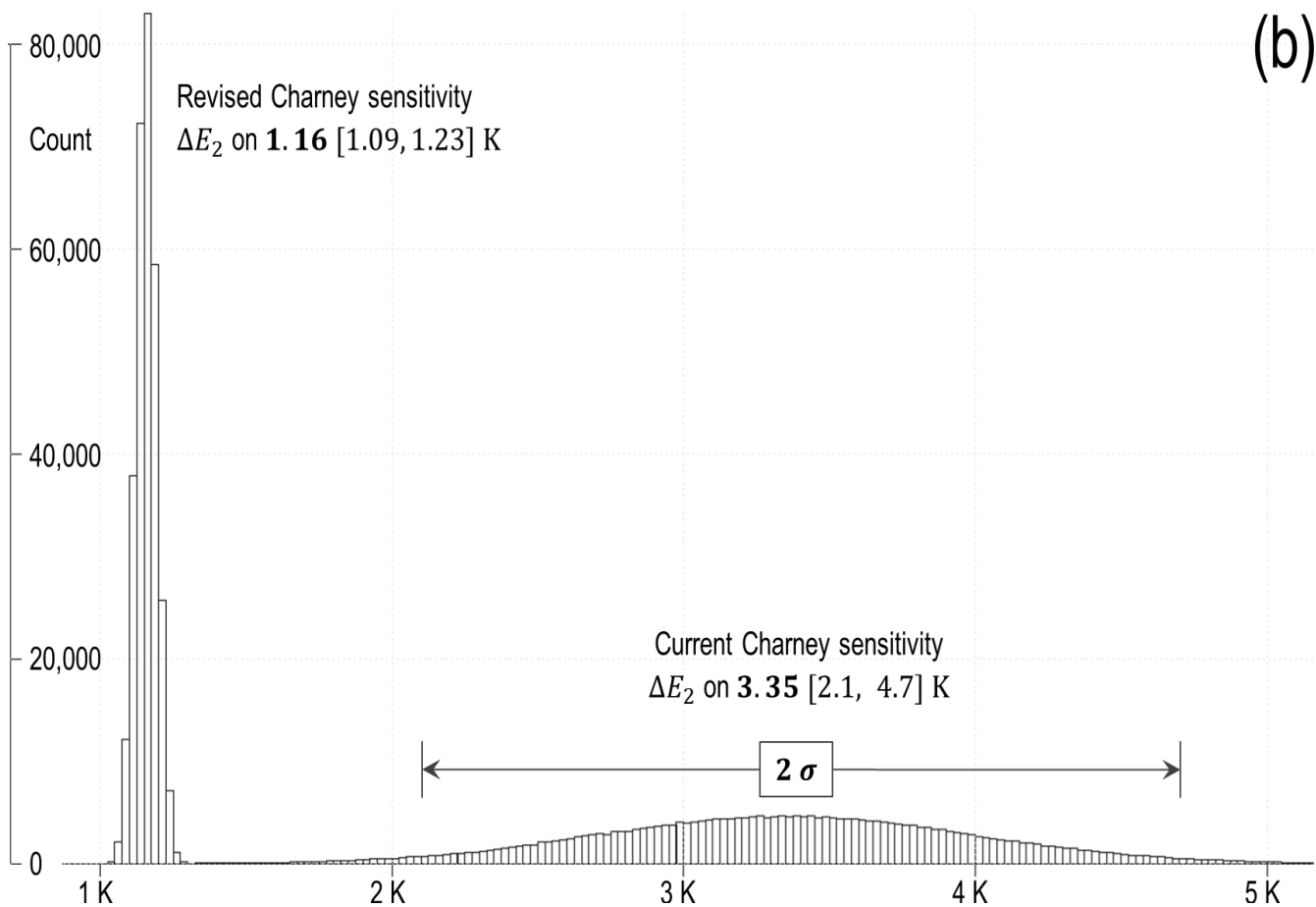
995
 996 **FIG. 9** A feedback amplifier with a μ gain block and a β feedback block (Bode 1945)



998
 999 **FIG. 10** The rectangular-hyperbolic response curves of Charney sensitivities ΔE_2 against
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 1002 since $\Delta(\Delta E_2)$ depends greatly on f_3 (Roe 2009, fig. 6). High-end predictions of ΔE_2 from
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 1004 from Eq. (1) are shown. Varying f_3 visibly makes very much more difference to ΔE_2 than
 1005 varying ΔR_2 , particularly where $f_3 \rightarrow 1$.
 1006

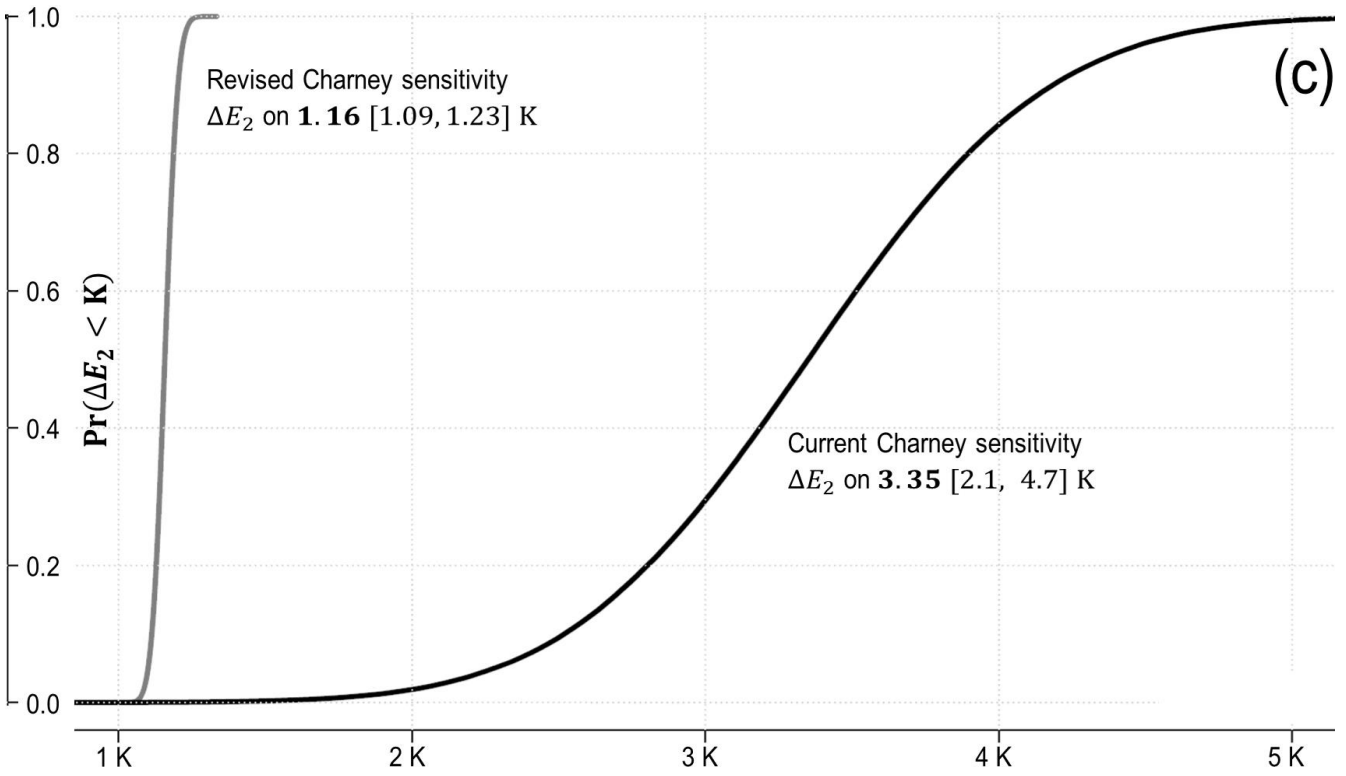


1007
1008 **FIG. 11 (a)** Monte Carlo distribution of Charney sensitivities ΔE_2 revised after correction
1009 of the error in defining temperature feedback identified herein. Bin widths are 0.005 K.



1010
1011 **FIG. 11 (b)** Scaled comparison of Monte Carlo distributions for revised (left) against
1012 current (right) Charney sensitivities ΔE_2 . Here, bin widths are 0.025 K.

1013



1014

1015 **FIG. 11 (c)** Cumulative distributions of probability that Charney sensitivity is less than a
1016 given value in K for revised (gray) against current (black) Charney sensitivities ΔE_2 .

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TABLES

TABLE 1 Current feedbacks based on IPCC (2013, p. 818, table 9.5 and p. 128, Fig. 1.2)

Temperature feedback	Lower bound	Mid-range	Upper bound	Timescale
Water vapor feedback $(\lambda_1)_2$	$+1.3 \text{ W m}^{-2} \text{ K}^{-1}$	$+1.6 \text{ W m}^{-2} \text{ K}^{-1}$	$+1.9 \text{ W m}^{-2} \text{ K}^{-1}$	Hours
Lapse rate feedback $(\lambda_2)_2$	$-1.0 \text{ W m}^{-2} \text{ K}^{-1}$	$-0.6 \text{ W m}^{-2} \text{ K}^{-1}$	$-0.2 \text{ W m}^{-2} \text{ K}^{-1}$	Hours
Cloud feedback $(\lambda_3)_2$	$-0.4 \text{ W m}^{-2} \text{ K}^{-1}$	$+0.3 \text{ W m}^{-2} \text{ K}^{-1}$	$+1.1 \text{ W m}^{-2} \text{ K}^{-1}$	Days
Surface albedo feedback $(\lambda_4)_2$	$+0.2 \text{ W m}^{-2} \text{ K}^{-1}$	$+0.3 \text{ W m}^{-2} \text{ K}^{-1}$	$+0.4 \text{ W m}^{-2} \text{ K}^{-1}$	Years
IPCC feedback sum $\lambda_2 = \sum_{i=1}^4 (\lambda_i)_2$	$+0.1 \text{ W m}^{-2} \text{ K}^{-1}$	$+1.6 \text{ W m}^{-2} \text{ K}^{-1}$	$+3.2 \text{ W m}^{-2} \text{ K}^{-1}$	Years
IPCC feedback fraction $f_2 = \lambda_2 P_2$	[+0.0]	+0.5	[+1.0]	
IPCC system-gain factor $a_2 = 1/(1 - f_2)$	[1.0]	2.0	[Undefined]	
IPCC implicit Charney sensi. $E_3 = \Delta R_2 a_2$	[1.0]	2.6	[∞]	

TABLE 2 Evolution of midrange reference temperature R_t (to the nearest 0.05 K).

Emission temperature	Pre-industrial	In 1850	1850-2011	In 2011	2011-2xCO ₂	At 2xCO ₂
R_0	ΔR_0	R_1	ΔR_1	R_2	ΔR_2	R_3
254.70 K	10.30 K	265.00 K	0.75 K	265.75 K	1.05 K	266.80 K

TABLE 3 Results from model 1

Emiss. temp.	Pre-industrial		In 1850		1850-2011		In 2011		2011 to 2xCO ₂		At 2xCO ₂		
R_0	254.70 K	ΔR_0	10.30 K	R_1	265.00 K	ΔR_1	0.75 K	R_2	265.75 K	ΔR_2	1.05 K	R_3	266.80 K
E_0	256.70 K	ΔE_0	30.85 K	E_1	287.55 K	ΔE_1	2.40 K	E_2	289.95 K	ΔE_2	3.40 K	E_3	293.30 K
b_0	2.00 K	Δb_0	20.55 K	b_1	22.55 K	Δb_1	1.65 K	b_2	24.20 K	Δb_2	2.35 K	b_3	26.50 K
f_0	0.0078	Δf_0	0.6663	f_1	0.0784	Δf_1	0.6858	f_2	0.0834	Δf_2	0.6889	f_3	0.0904
A_0	1.0078	ΔA_0	2.9966	A_1	1.0851	ΔA_1	3.1831	A_2	1.0910	ΔA_2	3.2149	A_3	1.0994
s_0	2.8297	(a_0)	(2.9966)	s_1	3.1700	(a_1)	(3.1831)	s_2	3.1963	(a_2)	(3.2149)	s_3	3.2335

TABLE 4 Results from model 2

Emiss. temp.	Pre-industrial		In 1850		1850-2011		In 2011		2011 to 2xCO ₂		At 2xCO ₂		
R_0	254.70 K	ΔR_0	10.30 K	R_1	265.00 K	ΔR_1	0.75 K	R_2	265.75 K	ΔR_2	1.05 K	R_3	266.80 K
E_0	261.95 K	ΔE_0	25.60 K	E_1	287.55 K	ΔE_1	1.95 K	E_2	289.50 K	ΔE_2	2.75 K	E_3	292.25 K
b_0	7.25 K	Δb_0	15.30 K	b_1	22.55 K	Δb_1	1.20 K	b_2	23.75 K	Δb_2	1.70 K	b_3	25.50 K
f_0	0.0277	Δf_0	0.5974	f_1	0.0784	Δf_1	0.6169	f_2	0.0821	Δf_2	0.6200	f_3	0.0872
A_0	1.0285	ΔA_0	2.4841	A_1	1.0851	ΔA_1	2.6105	A_2	1.0894	ΔA_2	2.6318	A_3	1.0955
s_0	2.3701	(a_0)	(2.4841)	s_1	2.6016	(a_1)	(2.6105)	s_2	2.6194	(a_2)	(2.6318)	s_3	2.6444

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TABLE 5 Results from model 3

Emiss. temp.	Pre-industrial	In 1850	1850-2011	In 2011	2011 to 2xCO ₂	At 2xCO ₂	
R_0	254.70 K ΔR_0	10.30 K R_1	265.00 K ΔR_1	0.75 K R_2	265.75 K ΔR_2	1.05 K R_3	266.80 K
E_0	274.30 K ΔE_0	13.25 K E_1	287.55 K ΔE_1	1.00 K E_2	288.55 K ΔE_2	1.40 K E_3	289.95 K
b_0	19.60 K Δb_0	2.95 K b_1	22.55 K Δb_1	0.25 K b_2	22.80 K Δb_2	0.35 K b_3	23.15 K
f_0	0.0715 Δf_0	0.2216 f_1	0.0784 Δf_1	0.2410 f_2	0.0790 Δf_2	0.2441 f_3	0.0798
A_0	1.0770 ΔA_0	1.2847 A_1	1.0851 ΔA_1	1.3175 A_2	1.0858 ΔA_2	1.3229 A_3	1.0867
s_0	1.2547 (a_0)	(1.2847) s_1	1.3152 (a_1)	(1.3175) s_2	1.3197 (a_2)	(1.3229) s_3	1.3261

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TABLE 6 Results from model 4

Emiss. temp.	Pre-industrial	In 1850	1850-2011	In 2011	2011 to 2xCO ₂	At 2xCO ₂	
R_0	254.70 K ΔR_0	10.30 K R_1	265.00 K ΔR_1	0.75 K R_2	265.75 K ΔR_2	1.05 K R_3	266.80 K
E_0	276.20 K ΔE_0	11.35 K E_1	287.55 K ΔE_1	0.85 K E_2	288.40 K ΔE_2	1.15 K E_3	289.55 K
b_0	21.50 K Δb_0	1.05 K b_1	22.55 K Δb_1	0.10 K b_2	22.65 K Δb_2	0.10 K b_3	22.75 K
f_0	0.0779 Δf_0	0.0915 f_1	0.0784 Δf_1	0.0918 f_2	0.0785 Δf_2	0.0918 f_3	0.0785
A_0	1.0845 ΔA_0	1.1007 A_1	1.0851 ΔA_1	1.1010 A_2	1.0852 ΔA_2	1.1011 A_3	1.0852
s_0	1.1004 (a_0)	(1.1007) s_1	1.1010 (a_1)	(1.1010) s_2	1.1010 (a_2)	(1.1011) s_3	1.1011

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TABLE 7 Results from model 5

Emiss. temp.	Pre-industrial	In 1850	1850-2011	In 2011	2011 to 2xCO ₂	At 2xCO ₂	
R_0	254.70 K ΔR_0	10.30 K R_1	265.00 K ΔR_1	0.75 K R_2	265.75 K ΔR_2	1.05 K R_3	266.80 K
E_0	276.35 K ΔE_0	11.20 K E_1	287.55 K ΔE_1	0.80 K E_2	288.35 K ΔE_2	1.15 K E_3	289.50 K
b_0	21.70 K Δb_0	0.90 K b_1	22.55 K Δb_1	0.05 K b_2	22.60 K Δb_2	0.10 K b_3	22.70 K
f_0	0.0784 Δf_0	0.0784 f_1	0.0784 Δf_1	0.0784 f_2	0.0784 Δf_2	0.0784 f_3	0.0784
A_0	1.0851 ΔA_0	1.0851 A_1	1.0851 ΔA_1	1.0851 A_2	1.0851 ΔA_2	1.0851 A_3	1.0851
s_0	1.0851 (a_0)	(1.0851) s_1	1.0851 (a_1)	(1.0851) s_2	1.0851 (a_2)	(1.0851) s_3	1.0851

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TABLE 8 Relationship between elevated ratios $\Delta f_0/f_0$ and elevated Charney sensitivities ΔE_2

Model	b_0	Δb_0	f_0	Δf_0	$\Delta f_0/f_0$	A_3	ΔE_2
CMIP5 current ΔE_2 : 1	2.00 K	20.55 K	0.0078	0.6663	85	1.0994	3.40 K
$b_t + 1.07\% K^{-1}$: 2	7.25 K	15.30 K	0.0277	0.5974	22	1.0955	2.75 K
IPCC anth. forcing: 3	19.60 K	2.95 K	0.0715	0.2216	3.1	1.0867	1.40 K
$R = 0 \Rightarrow b = 0$: 4	21.50 K	1.05 K	0.0779	0.0915	1.2	1.0852	1.15 K
Linear: 5	21.70 K	0.90 K	0.0784	0.0784	1.0	1.0851	1.15 K

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TABLE 9 System-gain factors A_2 and Charney sensitivities ΔE_2 in the industrial era to 2011

		ΔQ_1	ΔN_1	ΔT_1	ΔR_1	ΔE_1	ΔE_1	a_2	A_2	ΔE_2	ΔE_2
		$-\text{W m}^{-2}$	$-\text{W m}^{-2}$		K			Unitless		K	K
Data source	Year	1	2	3	4	5	6	7	8	9	10
Miller 2014	2012	2.95	0.60	0.76	0.91	2.88	0.95	1.04	1.085	1.11	1.15
Myhre 2017	2016	3.10	0.60	0.84	0.96	3.03	1.04	1.08	1.085	1.16	1.15
IPCC AR5 2013	1980	1.25	0.40	0.38	0.39	1.22	0.56	1.44	1.086	1.54	1.15
Knutti 2002	2001	1.90	0.50	0.62	0.59	1.86	0.84	1.43	1.086	1.53	1.15
IPCC AR5 2013	1950	0.57	0.20	0.26	0.18	0.56	0.40	2.27	1.086	2.42	1.15
IPCC AR5 2013	2011	2.29	0.60	0.76	0.71	2.24	1.03	1.45	1.086	1.55	1.15
Haywood 2007	2006	1.93	0.50	0.68	0.60	1.88	0.92	1.53	1.086	1.64	1.15
IPCC AR4 2007	2005	1.60	0.50	0.67	0.50	1.56	0.97	1.96	1.087	2.10	1.15
Skeie 2011	2010	1.40	0.60	0.74	0.43	1.37	1.30	2.98	1.088	3.19	1.15
Boucher 2001	2000	1.00	0.50	0.58	0.31	0.98	1.16	3.74	1.088	4.00	1.15

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Col. 1: Net anthropogenic forcing ΔQ_1 to year shown, given by the listed source authority;

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Col. 2: Estimated radiative imbalance ΔN_1 (based on Smith et al., 2015);

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Col. 3: Observed warming ΔT_1 from 1850 to the end year shown (Morice et al., 2012);

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Col. 4: Period reference sensitivity $\Delta R_1 = \Delta Q_1 P_2$;

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Col. 5: Current period equilibrium sensitivity $\Delta E_1 = \Delta R_1 (A_M)_2 \quad | \quad (A_M)_2 = 3.14$;

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Col. 6: Revised period equilibrium sensitivity $\Delta E_1 (= \Delta T_1 \Delta Q_1 / (\Delta Q_1 - \Delta N_1))$;

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Col. 7: Current system-gain factor $a_2 \approx \Delta E_1 / \Delta R_1$ (i.e., Col. 5 / Col. 4);

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Col. 8: Revised system-gain function $A_2 \approx E_2 / R_2$;

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Col. 9: Current Charney sensitivity $\Delta E_2 = \Delta Q_2 P_2 a_2$ (i.e., $\Delta Q_2 P_2 \times$ Col. 7); and

1053

Col. 10: Revised Charney sensitivity $\Delta E_2 = \Delta Q_2 P_2 A_2$ (i.e., $\Delta Q_2 P_2 \times$ Col. 8), to nearest 0.05 K.

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FIGURE CAPTIONS

FIG. 1. Overlapping projections by IPCC (2013) and CMIP5 (Andrews et al. 2012) of global warming from 1850-2011 (**blue scale**), in response to doubled CO₂ (**red scale**) and the sum of these two (**black scale**) greatly exceed warming equivalent to the 0.75 K observed from 1850-2011 (HadCRUT4: **green needle**). The 3.35 K CMIP5 mid-range Charney sensitivity (**red needle**) implies 2.4 K anthropogenic warming by 2011, about thrice observation. The revised warming interval derived herein (**pale green region**) is consistent with observed warming to 2011 (**green needle**).

FIG. 2. The *feedback loop* (a) simplifies to (b), the schematic for the **system-gain factor** A_t at time t . The *reference signal* (**reference temperature** R_t), the sum of the *input signal* (**emission temperature** R_0), and all *perturbations* (**reference sensitivities** $\Delta R_0, \dots, \Delta R_{t-1}$), is input via the *summative input/output node* to the feedback loop. The *output signal* (**equilibrium temperature** E_t), is the sum of R_t and the **feedback response** $b_t := f_t E_t$ ($:= E_t - R_t$). Then $A_t (= E_t/R_t)$ is equal to the sum $\sum_{i=0}^{\infty} f_t^i = (1 - f_t)^{-1}$ of the infinite convergent geometric series $\{f_t^0 + f_t^1 + \dots + f_t^{\infty}\}$ under the convergence criterion $|f_t| < 1$. The *feedback block* (a) and the *system-gain block* (b) must perform act not only on the anthropogenic perturbation ΔR_{t-1} but on the entire reference signal R_t .

FIG. 3 Specific humidity (g kg^{-1}) at 300, 600 and 1000 mb

FIG. 4 GCMs' projected "hot spot"²⁸ (a) is absent in observational data¹¹ (b). Temperature anomalies (in Kelvin) are color-coded.

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FIG. 6 Evolution of the feedback fraction f_t from emission temperature R_0 ($= 254.7$ K) to reference temperature R_1 ($= 265.00$ K) in 1850 and beyond.

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